

Hidraulička analiza funkcioniranja vodospremnika s preljevom i ispustom za vremenski promjenjiv dotok

Galić, Mila

Undergraduate thesis / Završni rad

2021

Degree Grantor / Ustanova koja je dodijelila akademski / stručni stupanj:

University of Split, Faculty of Civil Engineering, Architecture and Geodesy / Sveučilište u Splitu, Fakultet građevinarstva, arhitekture i geodezije

Permanent link / Trajna poveznica: <https://urn.nsk.hr/urn:nbn:hr:123:303022>

Rights / Prava: [In copyright](#)/[Zaštićeno autorskim pravom.](#)

Download date / Datum preuzimanja: **2025-02-28**

Repository / Repozitorij:



[FCEAG Repository - Repository of the Faculty of Civil Engineering, Architecture and Geodesy, University of Split](#)



UNIVERSITY OF SPLIT



DIGITALNI AKADEMSKI ARHIVI I REPOZITORIJI

SVEUČILIŠTE U SPLITU
FAKULTET GRAĐEVINARSTVA, ARHITEKTURE I
GEODEZIJE

ZAVRŠNI RAD

Mila Galić

Split, srpanj 2021.

SVEUČILIŠTE U SPLITU
FAKULTET GRAĐEVINARSTVA, ARHITEKTURE I GEODEZIJE

**Hidraulička analiza funkcioniranja vodospremnika
s preljevom i ispustom za vremenski promjenjiv dotok**

Završni rad

SVEUČILIŠTE U SPLITU

FAKULTET GRAĐEVINARSTVA, ARHITEKTURE I GEODEZIJE

Split, Matice hrvatske 15

STUDIJ: **PREDDIPLOMSKI SVEUČILIŠNI STUDIJ
GRAĐEVINARSTVA**

KANDIDAT: **Mila Galić**

BROJ INDEKSA: **4564**

KATEDRA: **Katedra za hidromehaniku i hidrauliku**

PREDMET: **Hidromehanika**

ZADATAK ZA ZAVRŠNI RAD

Tema: Hidraulička analiza funkcioniranja vodospremnika s preljevom i ispustom za vremenski promjenjiv dotok

Opis zadatka: Potrebno je izvesti proračun razine vodostaja ovisno o vremenu, te ga riješiti preko numeričke integracije mješovitim postupkom.

Zadatak treba riješiti za 3 različite širine preljeva, te istražiti utjecaj veličine vremenskog koraka na kvalitetu rješenja.

Rezultate prikazati grafički i tablično (proračun provesti u EXCELL-u)

U Splitu, 15. lipnja 2021.

Voditelj Završnog rada:

Doc. dr. sc. Davor Bojanić, dipl.ing.građ.

IZJAVA

Završni rad sam izradila samostalno, u suradnji s mentorom poštivala sam sve građevinske propise iz područja građevinarstva. Fakultet građevinarstva arhitekture i geodezije polaže sva prava intelektualnog vlasništva na ovaj rad.

Mila Galić

U Splitu, _____ 2021.

Zahvaljujem se svim djelnicima Fakulteta Građevinarstva, arhitekture i geodezije u Splitu, te se posebno zahvaljujem mentoru doc.dr.sc. Davoru Bojaniću na korisnim savjetima, ukazanoj podršci i velikom razumijevanju .

Veliko hvala svim mojim prijateljima, kolegama, planinarima bez kojih sve ove godine nebi bile iste.

Na kraju, želim se zahvaliti trima najvažnijim osobama majci, ocu i sestri bez čije podrške i ljubavi ne bih bila ovdje danas. Naučili su me kako da budem jaka, odlučna, neovisna, čvrstog stava i karaktera, te ono najvažnije da ulagati u sebe znači ulagati u svoje obrazovanje.

Hidraulička analiza funkcioniranja vodospremnika s preljevom i ispustom za vremenski promjenjiv dotok

Sažetak:

U ovom radu je, za zadani otvoreni vodospremnik s preljevom i ispustom, izvršen proračun razine vode u vodospremniku u funkciji vremena, numeričkom integracijom mješovitim postupkom.

Zadatak je riješen za 3 različite širine preljeva te je istražen utjecaj veličine vremenskog koraka na kvalitetu rješenja.

Ključne riječi:

Vremenski promjenjiv dotok, numerička integracija, mješoviti postupak, otvoreni spremnik, preljev...

The hydraulic analysis of reservoir functioning with overflow and discharge for a time-varying inflow

Abstract:

In this paper, for a given open reservoir with overflow and discharge, the water level is calculated depending on the time by numerical integration by a mixed procedure.

The problem was solved for 3 different overflow widths and the influence of the time step size on the solution quality was investigated.

Key words: time-varying inflow, numerical integration, mixed process, open tank, overflow...

SADRŽAJ

1. Zadatak za završni rad:	8
2. Tehnički opis:.....	10
2.1. Uvod:.....	10
2.2. Značajne geometrijske i hidrauličke karakteristike.....	10
3. Proračun vodospremnika:	11
3.1. Postupak proračuna vodospremnika:	11
3.2. Rezultati proračuna vodostaja u vodospremi	14
3.2.1. Rezultati za zadane širine preljevnih pragova.....	14
3.3. Grafički prikaz rezultata.....	24
4. Utjecaj vremenskog koraka.....	27
5. Zaključak :	29
6. Literatura :.....	29

Popis slika :

Slika 1 Zadani vodospremnik s ispusnom cijevi i preljevom	10
Slika 2 Realizacija Newtonove metode	12
Slika 3 Prikaz vodostaja za B_1, B_2, B_3	24
Slika 4 Prikaz dotoka, protoka kroz kratku cijev i preljevnog protoka za širinu preljevnog praga $B=2m$ ovisno o vremenu.....	24
Slika 5 Prikaz dotoka, protoka kroz kratku cijev i preljevnog protoka za širinu preljevnog praga $B=3m$ ovisno o vremenu.....	25
Slika 6 Prikaz dotoka , protoka kroz kratku cijev i preljevnog protoka za širinu preljevnog praga $B=4m$ ovisno o vremenu.....	25
Slika 7 Prikaz dotoka za sve širine preljevnog praga ovisno o vremenu	26
Slika 8 Prikaz protoka kroz kratku cijev za sve širine preljevnog praga ovisno o vremenu.....	26
Slika 9 Prikaz preljevnog protoka za sve širine preljevnog praga ovisno o vremenu.....	27
Slika 10 Prikaz vodostaja za $B=2m$ za različite vremenske korake.....	27
Slika 11 Prikaz protoka kroz kratku cijev $B=2m$ za različite vremenske korake	28
Slika 12 Prikaz preljevnog protoka $B=2m$ za različite vremenske korake	28

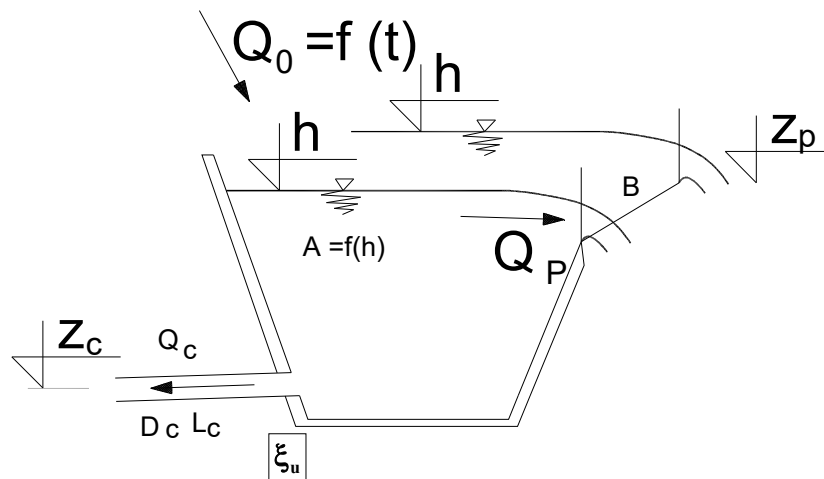
1. Zadatak za završni rad:

Zadan je otvoreni spremnik čija je površina promjenjiva ovisno o vodostaju u njemu. U spremnik se ulijeva protok vode koji je funkcija vremena. Iz spremnika voda istječe slobodno u atmosferu kroz kratku cijev. Na spremniku, na koti z_p postoji preljev širine B_p . Preko preljeva se prelijeva višak vode iz spremnika.

Studentica će postaviti sve potrebne jednadžbe koje opisuju zadani problem. Zadatak će riješiti numeričkom integracijom mješovitim postupkom.

Zadatak treba riješiti za 3 varijante širine preljeva. Potrebno je analizirati utjecaj veličine vremenskog koraka na kvalitetu rješenja.

Za rješavanje koristiti tablični kalkulator (EXCELL). Rezultate prikazati grafički i tablično.



Slika 1. Vodospremnik s preljevom i ispustom

Zadano je:

Površina vodospremnika u funkciji nadmorske visine:

h (m n.m.)	A (m ²)
90	300
100	450
105	800
110	1200

Dotok u vodospremnik:

t (s)	Q ₀ (m ³ /s)
0,00	1,50
200,00	2,30
300,00	8,00
500,00	10,00
900,00	3,00
1200,00	1,50
10000,00	1,50

$D_c=0.6$ (m)

$L_c=50.0$ (m)

$\varepsilon = 0.001$ (m)

$\nu = 0.00000131$ (m²/s)

$\xi_u = 0.5$

$B_1=2.0$ (m); $B_2=3.0$ (m); $B_3=4.0$ (m)

$z_p = 100.00$ (m n. m.)

$\Theta=0.5$

$L=1.1$

Početna razina vode u prvom spremniku je 99.50 (m n.m.).

Split, 15. lipnja 2021.

Doc. dr. sc. Davor Bojanić

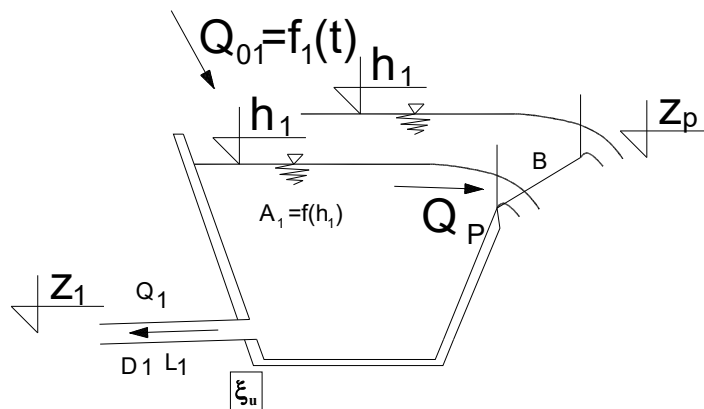
2. Tehnički opis:

2.1. Uvod:

Zadatkom je zadan otvoreni spremnik čija je površina definirana u funkciji nadmorske visine. Iz otvorenog spremnika voda istječe slobodno u atmosferu kroz kratku cijev, a ostatak vode se počinje prelijevati kada razina vode u vodospremniku prijeđe visinu krune preljevnog praga. Na temelju zadanih podataka istražen je utjecaj veličine vremenskog koraka na kvalitetu rješenja za tri varijante dužine preljevnog praga.

Zadano je:

- Površina vodospremnika u funkciji nadmorske visine
- Dotok u funkciji vremena
- Početna razina vode u vodospremniku
- Kota krune preljevnog praga



Slika 1 Zadani vodospremnik s ispusnom cijevi i preljevom

2.2. Značajne geometrijske i hidrauličke karakteristike

Zadani sustav sastoji se od otvorenog spremnika s dotokom promjenjivim u vremenu, a pri dnu spremnika nalazi se kratka cijev kroz koju voda slobodno istječe u atmosferu. Površina vodospremnika se mijenja ovisno o nadmorskoj visini. Na nadmorskoj visini $h=90.0$ (m n.m.) površina vodospremnika iznosi $A=300$ (m^2), za $h=100.0$ (m n.m.) površina iznosi $A=450$ (m^2), za $h=105.0$ (m n.m.) površina iznosi $A=800$ (m^2) i za $h=110.0$ (m n.m.) površina vodospremnika iznosi $A=1200$ (m^2). Krana preljevnog praga nalazi se na

koti $Z_p=100$ (m n.m.). Cijev kroz koju istječe voda nalazi se na koti $Z_1=90$ (m n.m.). Duljina cijevi iznosi $L_1=50$ (m), a dijametar cijevi iznosi $D_c=0.6$ (m).

Za koeficijent lokalnog gubitka energije na ulazu uzeta je vrijednost $\xi_u=0.5$. Zadatom je zadana apsolutna pogonska hidraulička hrapavost u iznosu od $\varepsilon=0.001$ (m), pomoću koje se izračunavaju linijski gubici energije. Također je zadana vrijednost i kinematičkog koeficijenta viskoznosti tekućine $\nu = 0.00000131$ (m^2/s).

3. Proračun vodospremnika:

3.1. Postupak proračuna vodospremnika:

Početna razina vode u vodospremniku je 99.50 (m n.m.).

1. Jednadžba kontinuiteta za vodospremnik je:

$$A \cdot \frac{dh}{dt} = Q_0 - Q_1 - Q_p \quad (1)$$

Nakon separacije varijabli dobije se:

$$dh = \frac{Q_0 - Q_1 - Q_p}{A} \cdot dt \quad (2)$$

Numerička integracija mješovitim postupkom daje:

$$h^{k+1} = h^k + \frac{Q_0^k - Q_1^k - Q_p^k}{A^k} \cdot (1 - \vartheta) \cdot \Delta t + \frac{Q_0^{k+1} - Q_1^{k+1} - Q_p^{k+1}}{A^{k+1}} \cdot \vartheta \cdot \Delta t \quad (3)$$

Pri čemu je A površina spremnika, Q_0 je dotok, Q_1 je protok kroz odvodnu cijev, dok je Q_p protok preko preljevnog praga.

h je vodostaj u vodospremniku.

Oznake h^k , Q_0^k , Q_1^k , Q_p^k i A^k odnose se na vrijednosti na početku vremenskog intervala. Oznake h^{k+1} , Q_0^{k+1} , Q_1^{k+1} , Q_p^{k+1} i A^{k+1} odnose se na vrijednosti na kraju vremenskog intervala. Vodostaj na kraju intervala odredit će se iz izraza (3).

2. Preljevni protok računa se prema sljedećem:

$$\text{ako je } h > z_p, Q_p = m \cdot B \cdot \sqrt{2g} \cdot (h - z_p)^{3/2} \quad (4)$$

$$\text{ako je } h = z_p, Q_p = 0.00 \quad (5)$$

$$\text{ako je } h < z_p, Q_p = 0.00 \quad (6)$$

Ukoliko je vodostaj u spremniku jednak ili manji od kote preljevnog praga, onda je preljevni protok jednak nuli (5, 6), a ukoliko je vodostaj u spremniku veći od kote krune preljevnog praga, onda se preljevni protok računa po datoj izrazu (4).

3. Protok kroz cijev:

$$Q_1 = \frac{1}{\sqrt{\xi_u + \lambda \frac{L_1}{D_1} + \alpha}} \sqrt{2g \cdot (h - z_1)} \cdot D_1^2 \cdot \frac{\pi}{4} \quad (7)$$

ako je $h = z_1$

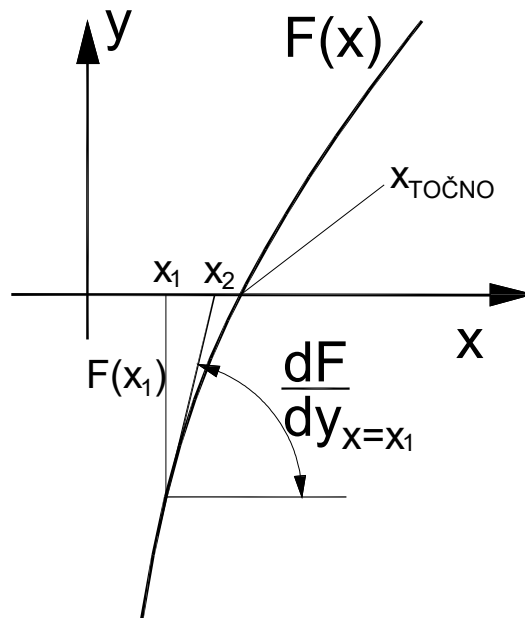
$$Q_1 = 0.0 \quad (8)$$

ako je $h < z_1$

$$Q_1 = 0.0 \frac{\pi}{4} \quad (9)$$

Jednadžba (3) je nelinearna jednadžba s jednom nepoznicom. Traži se h^{k+1} , tj. vodostaj na kraju vremenskog koraka.

Primjenjuje se Newtonova metoda za rješavanje nelinearnih jednadžbi.



Slika 2 Realizacija Newtonove metode

Neka je zadana funkcija $F(x)$. Tražimo onaj x ($x_{\text{točno}}$) za kojeg vrijedi da je $F(x)=0.0$. Postupak je takav da se odabere vrijednost x_1 . Za tu vrijednost x_1 izračuna se vrijednost funkcije u toj točki $F(x_1)$ i vrijednost derivacije u toj točki. Novu vrijednost za x , tj. x_2 koja će biti bliže točnom rješenju dobit će se iz sljedećeg:

$$(x_2 - x_1) \cdot \frac{dF}{dy}_{x=x_1} = -F(x_1) \quad (10)$$

Oдавde slijedi:

$$x_2 = x_1 - \frac{F(x_1)}{\frac{dF}{dy}_{x=x_1}} \quad (11)$$

Time je određen postupak postupnog približavanja točnom rješenju.

Formira se funkcija F . Ovdje je nezavisna varijabla vodostaj h^{k+1} .

$$F = h^{k+1} - h^k - \frac{Q_0^k - Q_1^k - Q_p^k}{A^k} \cdot (1 - \vartheta) \cdot \Delta t - \frac{Q_0^{k+1} - Q_1^{k+1} - Q_p^{k+1}}{A^{k+1}} \cdot \vartheta \cdot \Delta t = 0 \quad (12)$$

$$Q_1^k = \frac{1}{\sqrt{\xi_u + \lambda^k \cdot \frac{L_1}{D_1} + \alpha}} \cdot \sqrt{2g \cdot (h^k - z_1)} \cdot D_1^2 \cdot \frac{\pi}{4} \quad (13)$$

$$Q_1^{k+1} = \frac{1}{\sqrt{\xi_u + \lambda^{k+1} \cdot \frac{L_1}{D_1} + \alpha}} \cdot \sqrt{2g \cdot (h^{k+1} - z_1)} \cdot D_1^2 \cdot \frac{\pi}{4} \quad (14)$$

$$\text{ako je } h^k > z_p, Q_p^k = m \cdot B \cdot \sqrt{2g} \cdot (h^k - z_p)^{3/2} \quad (15)$$

$$\text{ako je } h^k = z_p, Q_p^k = 0.00 \quad (16)$$

$$\text{ako je } h^k < z_p, Q_p^k = 0.00 \quad (17)$$

$$\text{ako je } h^{k+1} > z_p, Q_p^{k+1} = m \cdot B \cdot \sqrt{2g} \cdot (h^{k+1} - z_p)^{3/2} \quad (18)$$

$$\text{ako je } h^{k+1} = z_p, Q_p^{k+1} = 0.00 \quad (19)$$

$$\text{ako je } h^{k+1} < z_p, Q_p^{k+1} = 0.00 \quad (20)$$

Derivacija funkcije F po h^{k+1} je:

$$\frac{dF}{dh^{k+1}} = 1.0 + \frac{\vartheta \cdot \Delta t}{A^{k+1}} \cdot \left(\frac{dQ_1^{k+1}}{dh^{k+1}} + \frac{dQ_p^{k+1}}{dh^{k+1}} \right) \quad (21)$$

$$\frac{dQ_1^{k+1}}{dh^{k+1}} = \frac{1}{\sqrt{\xi_u + \lambda^{k+1} \cdot \frac{L_1}{D_1} + \alpha}} \cdot \sqrt{2g} \cdot D_1^2 \cdot \frac{\pi}{4} \cdot \frac{1}{2 \cdot \sqrt{(h^{k+1} - z_1)}} \quad (22)$$

$$\text{ako je } h^{k+1} > z_p, \frac{dQ_p^{k+1}}{dh^{k+1}} = m \cdot B \cdot \sqrt{2g} \cdot \frac{3}{2} \cdot (h^{k+1} - z_p)^{1/2} \quad (23)$$

$$\text{ako je } h^{k+1} = z_p, \frac{dQ_p^{k+1}}{dh^{k+1}} = 0.00 \quad (24)$$

$$\text{ako je } h^{k+1} < z_p, \frac{dQ_p^{k+1}}{dh^{k+1}} = 0.00 \quad (25)$$

$$h^{k+1,n} = h^{k+1} + \Delta h^{k+1} \quad (26)$$

$$h^{k+1,n} = h^{k+1} - \frac{F}{\frac{dF}{dh^{k+1}}} \quad (27)$$

Postupak se ponavlja sve dok prirast $\left(\frac{-F}{\frac{dF}{dh^{k+1}}} \right)$ po apsolutnoj vrijednosti ne bude manji od zadane točnosti.

Kad se to postigne ide se na novi vremenski interval.

3.2. Rezultati proračuna vodostaja u vodospremi

Rezultati su dobiveni rješenjem nelinearne jednadžbe opisane u točki 3.1. Rješenje je provedeno u programu “Microsoft Excell” na sljedeći način:

Numeričkom integracijom mješovitim postupkom dobiveni su sljedeći podaci o razini vode u vodospremniku, protoku kroz kratku cijev, te preljevnom protoku, ovisno o vremenu, za zadane različite širine preljevnog praga ($B_1 = 2m, B_2 = 3m, B_3 = 4m$).

3.2.1. Rezultati za zadane širine preljevnih pragova

U tablici 1. prikazani su rezultati proračuna za dužinu preljevnog praga od 2 (m), i vremenski korak od 5 (s).

U tablici 2. prikazani su rezultati proračuna za dužinu preljevnog praga od 3 (m), i vremenski korak od 5 (s).

U tablici 3. prikazani su rezultati proračuna za dužinu preljevnog praga od 4 (m), i vremenski korak od 5 (s).

Tablica 1 Rezultati proračuna za dužinu preljevog praga $B_1 = 2 \text{ m}$

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
0	99,5000	1,5000	0,0000	2,0739
5	99,4936	1,5200	0,0000	2,0732
10	99,4875	1,5400	0,0000	2,0725
15	99,4816	1,5600	0,0000	2,0719
20	99,4759	1,5800	0,0000	2,0713
25	99,4705	1,6000	0,0000	2,0707
30	99,4653	1,6200	0,0000	2,0701
35	99,4603	1,6400	0,0000	2,0695
40	99,4556	1,6600	0,0000	2,0690
45	99,4510	1,6800	0,0000	2,0685
50	99,4468	1,7000	0,0000	2,0681
55	99,4427	1,7200	0,0000	2,0676
60	99,4389	1,7400	0,0000	2,0672
65	99,4353	1,7600	0,0000	2,0668
70	99,4319	1,7800	0,0000	2,0664
75	99,4288	1,8000	0,0000	2,0661
80	99,4259	1,8200	0,0000	2,0658
85	99,4232	1,8400	0,0000	2,0655
90	99,4208	1,8600	0,0000	2,0652
95	99,4186	1,8800	0,0000	2,0650
100	99,4166	1,9000	0,0000	2,0648
105	99,4149	1,9200	0,0000	2,0646
110	99,4133	1,9400	0,0000	2,0644
115	99,4120	1,9600	0,0000	2,0643
120	99,4110	1,9800	0,0000	2,0641
125	99,4101	2,0000	0,0000	2,0640
130	99,4095	2,0200	0,0000	2,0640
135	99,4091	2,0400	0,0000	2,0639
140	99,4090	2,0600	0,0000	2,0639
145	99,4090	2,0800	0,0000	2,0639
150	99,4093	2,1000	0,0000	2,0640
155	99,4099	2,1200	0,0000	2,0640
160	99,4106	2,1400	0,0000	2,0641
165	99,4116	2,1600	0,0000	2,0642
170	99,4128	2,1800	0,0000	2,0643
175	99,4142	2,2000	0,0000	2,0645
180	99,4159	2,2200	0,0000	2,0647
185	99,4177	2,2400	0,0000	2,0649
190	99,4198	2,2600	0,0000	2,0651
195	99,4221	2,2800	0,0000	2,0654
200	99,4247	2,3000	0,0000	2,0656
205	99,4289	2,5850	0,0000	2,0661
210	99,4364	2,8700	0,0000	2,0669
215	99,4471	3,1550	0,0000	2,0681
220	99,4610	3,4400	0,0000	2,0696
225	99,4781	3,7250	0,0000	2,0715
230	99,4984	4,0100	0,0000	2,0737
235	99,5219	4,2950	0,0000	2,0763
240	99,5485	4,5800	0,0000	2,0792
245	99,5783	4,8650	0,0000	2,0824
250	99,6112	5,1500	0,0000	2,0860

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
255	99,6473	5,4350	0,0000	2,0899
260	99,6864	5,7200	0,0000	2,0942
265	99,7287	6,0050	0,0000	2,0987
270	99,7740	6,2900	0,0000	2,1036
275	99,8224	6,5750	0,0000	2,1088
280	99,8739	6,8600	0,0000	2,1143
285	99,9283	7,1450	0,0000	2,1202
290	99,9858	7,4300	0,0000	2,1263
295	100,0459	7,7150	0,0348	2,1327
300	100,1078	8,0000	0,1254	2,1392
305	100,1698	8,0500	0,2478	2,1458
310	100,2302	8,1000	0,3913	2,1522
315	100,2889	8,1500	0,5503	2,1583
320	100,3459	8,2000	0,7208	2,1643
325	100,4010	8,2500	0,8997	2,1701
330	100,4542	8,3000	1,0847	2,1756
335	100,5056	8,3500	1,2738	2,1810
340	100,5551	8,4000	1,4654	2,1861
345	100,6027	8,4500	1,6581	2,1910
350	100,6486	8,5000	1,8508	2,1958
355	100,6926	8,5500	2,0427	2,2003
360	100,7350	8,6000	2,2329	2,2047
365	100,7757	8,6500	2,4208	2,2088
370	100,8147	8,7000	2,6060	2,2128
375	100,8522	8,7500	2,7880	2,2167
380	100,8883	8,8000	2,9665	2,2204
385	100,9228	8,8500	3,1414	2,2239
390	100,9560	8,9000	3,3123	2,2273
395	100,9879	8,9500	3,4792	2,2305
400	101,0184	9,0000	3,6421	2,2336
405	101,0478	9,0500	3,8008	2,2366
410	101,0760	9,1000	3,9553	2,2394
415	101,1032	9,1500	4,1058	2,2422
420	101,1292	9,2000	4,2521	2,2448
425	101,1543	9,2500	4,3944	2,2473
430	101,1784	9,3000	4,5328	2,2498
435	101,2016	9,3500	4,6673	2,2521
440	101,2239	9,4000	4,7980	2,2544
445	101,2454	9,4500	4,9251	2,2565
450	101,2662	9,5000	5,0486	2,2586
455	101,2861	9,5500	5,1686	2,2606
460	101,3054	9,6000	5,2854	2,2625
465	101,3241	9,6500	5,3989	2,2644
470	101,3421	9,7000	5,5094	2,2662
475	101,3595	9,7500	5,6168	2,2679
480	101,3763	9,8000	5,7215	2,2696
485	101,3926	9,8500	5,8234	2,2712
490	101,4084	9,9000	5,9227	2,2728
495	101,4237	9,9500	6,0194	2,2743
500	101,4385	10,0000	6,1138	2,2758
505	101,4523	9,9125	6,2020	2,2772

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
510	101,4645	9,8250	6,2805	2,2784
515	101,4753	9,7375	6,3497	2,2795
520	101,4846	9,6500	6,4101	2,2804
525	101,4926	9,5625	6,4621	2,2812
530	101,4994	9,4750	6,5063	2,2819
535	101,5051	9,3875	6,5429	2,2824
540	101,5096	9,3000	6,5725	2,2829
545	101,5131	9,2125	6,5954	2,2832
550	101,5156	9,1250	6,6119	2,2835
555	101,5172	9,0375	6,6225	2,2836
560	101,5180	8,9500	6,6276	2,2837
565	101,5180	8,8625	6,6273	2,2837
570	101,5172	8,7750	6,6220	2,2836
575	101,5156	8,6875	6,6120	2,2835
580	101,5134	8,6000	6,5976	2,2833
585	101,5106	8,5125	6,5791	2,2830
590	101,5072	8,4250	6,5567	2,2826
595	101,5032	8,3375	6,5306	2,2822
600	101,4986	8,2500	6,5010	2,2818
605	101,4936	8,1625	6,4682	2,2813
610	101,4881	8,0750	6,4323	2,2807
615	101,4821	7,9875	6,3936	2,2801
620	101,4757	7,9000	6,3522	2,2795
625	101,4689	7,8125	6,3083	2,2788
630	101,4617	7,7250	6,2620	2,2781
635	101,4541	7,6375	6,2135	2,2774
640	101,4462	7,5500	6,1630	2,2766
645	101,4380	7,4625	6,1104	2,2758
650	101,4294	7,3750	6,0561	2,2749
655	101,4206	7,2875	6,0000	2,2740
660	101,4115	7,2000	5,9424	2,2731
665	101,4021	7,1125	5,8832	2,2722
670	101,3925	7,0250	5,8227	2,2712
675	101,3826	6,9375	5,7608	2,2702
680	101,3725	6,8500	5,6977	2,2692
685	101,3621	6,7625	5,6335	2,2682
690	101,3516	6,6750	5,5682	2,2671
695	101,3408	6,5875	5,5019	2,2661
700	101,3299	6,5000	5,4346	2,2650
705	101,3188	6,4125	5,3665	2,2639
710	101,3074	6,3250	5,2976	2,2627
715	101,2960	6,2375	5,2279	2,2616
720	101,2843	6,1500	5,1575	2,2604
725	101,2725	6,0625	5,0864	2,2592
730	101,2605	5,9750	5,0148	2,2580
735	101,2484	5,8875	4,9426	2,2568
740	101,2361	5,8000	4,8698	2,2556
745	101,2237	5,7125	4,7966	2,2543
750	101,2111	5,6250	4,7229	2,2531
755	101,1984	5,5375	4,6488	2,2518
760	101,1856	5,4500	4,5744	2,2505

Tablica 1- nastavak 1 - Rezultati proračuna za dužinu preljevog praga $B_1 = 2 \text{ m}$

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
765	101,1726	5,3625	4,4996	2,2492
770	101,1595	5,2750	4,4244	2,2479
775	101,1463	5,1875	4,3490	2,2465
780	101,1330	5,1000	4,2733	2,2452
785	101,1195	5,0125	4,1974	2,2438
790	101,1059	4,9250	4,1212	2,2425
795	101,0922	4,8375	4,0449	2,2411
800	101,0784	4,7500	3,9684	2,2397
805	101,0645	4,6625	3,8918	2,2383
810	101,0504	4,5750	3,8150	2,2368
815	101,0363	4,4875	3,7381	2,2354
820	101,0220	4,4000	3,6611	2,2340
825	101,0076	4,3125	3,5841	2,2325
830	100,9931	4,2250	3,5069	2,2310
835	100,9785	4,1375	3,4298	2,2296
840	100,9637	4,0500	3,3526	2,2281
845	100,9489	3,9625	3,2755	2,2265
850	100,9339	3,8750	3,1983	2,2250
855	100,9189	3,7875	3,1211	2,2235
860	100,9037	3,7000	3,0440	2,2219
865	100,8883	3,6125	2,9670	2,2204
870	100,8729	3,5250	2,8900	2,2188
875	100,8574	3,4375	2,8131	2,2172
880	100,8417	3,3500	2,7363	2,2156
885	100,8259	3,2625	2,6596	2,2140
890	100,8100	3,1750	2,5830	2,2124
895	100,7939	3,0875	2,5066	2,2107
900	100,7777	3,0000	2,4304	2,2091
905	100,7617	2,9125	2,3537	2,2074
910	100,7462	2,8250	2,2839	2,2058
915	100,7310	2,7375	2,2149	2,2043
920	100,7163	2,6500	2,1484	2,2028
925	100,7020	2,5625	2,0843	2,2013
930	100,6881	2,4750	2,0224	2,1998
935	100,6745	2,3875	1,9628	2,1984
940	100,6612	2,3000	1,9051	2,1971
945	100,6482	2,2125	1,8493	2,1957
950	100,6355	2,1250	1,7953	2,1944
955	100,6231	2,0375	1,7430	2,1931
960	100,6110	1,9500	1,6923	2,1919
965	100,5991	1,8625	1,6431	2,1907
970	100,5874	1,7750	1,5954	2,1895
975	100,5760	1,6875	1,5490	2,1883
980	100,5647	1,6000	1,5038	2,1871
985	100,5537	1,5125	1,4599	2,1860
990	100,5428	1,4250	1,4172	2,1848
995	100,5321	1,3375	1,3755	2,1837
1000	100,5216	1,2500	1,3348	2,1826
1005	100,5112	1,1625	1,2952	2,1816
1010	100,5010	1,0750	1,2564	2,1805
1015	100,4909	0,9875	1,2186	2,1794
1020	100,4809	0,9000	1,1816	2,1784
1025	100,4710	0,8125	1,1454	2,1774
1030	100,4612	0,7250	1,1100	2,1764
1035	100,4516	0,6375	1,0753	2,1754
1040	100,4420	0,5500	1,0413	2,1744
1045	100,4325	0,4625	1,0080	2,1734
1050	100,4231	0,3750	0,9754	2,1724
1055	100,4138	0,2875	0,9433	2,1714
1060	100,4046	0,2000	0,9118	2,1704
1065	100,3954	0,1125	0,8809	2,1695
1070	100,3862	0,0250	0,8506	2,1685
1075	100,3771	0,1375	0,8207	2,1676
1080	100,3681	0,2500	0,7914	2,1666
1085	100,3591	0,3625	0,7626	2,1657
1090	100,3501	0,4750	0,7342	2,1648
1095	100,3412	0,5875	0,7063	2,1638
1100	100,3323	0,7000	0,6788	2,1629
1105	100,3234	0,8125	0,6518	2,1620
1110	100,3146	0,9250	0,6252	2,1610

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
1115	100,3057	1,0375	0,5990	2,1601
1120	100,2969	1,1500	0,5732	2,1592
1125	100,2880	1,2625	0,5478	2,1583
1130	100,2792	1,3750	0,5227	2,1573
1135	100,2703	1,4875	0,4981	2,1564
1140	100,2615	1,6000	0,4738	2,1555
1145	100,2526	1,7125	0,4500	2,1545
1150	100,2438	1,8250	0,4265	2,1536
1155	100,2349	1,9375	0,4033	2,1527
1160	100,2259	2,0500	0,3806	2,1517
1165	100,2170	2,1625	0,3582	2,1508
1170	100,2080	2,2750	0,3362	2,1498
1175	100,1990	2,3875	0,3146	2,1489
1180	100,1899	2,5000	0,2933	2,1479
1185	100,1808	2,6125	0,2725	2,1470
1190	100,1717	2,7250	0,2521	2,1460
1195	100,1625	2,8375	0,2321	2,1450
1200	100,1532	2,9500	0,2125	2,1441
1205	100,1440	3,0625	0,1937	2,1431
1210	100,1350	3,1750	0,1758	2,1421
1215	100,1262	3,2875	0,1589	2,1412
1220	100,1176	3,4000	0,1429	2,1403
1225	100,1091	3,5125	0,1277	2,1394
1230	100,1008	3,6250	0,1134	2,1385
1235	100,0927	3,7375	0,0999	2,1376
1240	100,0846	3,8500	0,0873	2,1368
1245	100,0768	3,9625	0,0754	2,1360
1250	100,0690	4,0750	0,0643	2,1351
1255	100,0614	4,1875	0,0539	2,1343
1260	100,0539	4,3000	0,0443	2,1335
1265	100,0464	4,4125	0,0355	2,1327
1270	100,0391	4,5250	0,0274	2,1320
1275	100,0319	4,6375	0,0202	2,1312
1280	100,0247	4,7500	0,0138	2,1304
1285	100,0176	4,8625	0,0083	2,1297
1290	100,0106	4,9750	0,0039	2,1289
1295	100,0036	5,0875	0,0008	2,1282
1300	99,9966	5,2000	0,0000	2,1274
1305	99,9896	5,3125	0,0000	2,1267
1310	99,9827	5,4250	0,0000	2,1260
1315	99,9757	5,5375	0,0000	2,1252
1320	99,9688	5,6500	0,0000	2,1245
1325	99,9618	5,7625	0,0000	2,1237
1330	99,9549	5,8750	0,0000	2,1230
1335	99,9479	5,9875	0,0000	2,1223
1340	99,9410	6,1000	0,0000	2,1215
1345	99,9341	6,2125	0,0000	2,1208
1350	99,9272	6,3250	0,0000	2,1200
1355	99,9203	6,4375	0,0000	2,1193
1360	99,9134	6,5500	0,0000	2,1186
1365	99,9065	6,6625	0,0000	2,1178
1370	99,8996	6,7750	0,0000	2,1171
1375	99,8928	6,8875	0,0000	2,1164
1380	99,8859	6,9999	0,0000	2,1156
1385	99,8790	7,1125	0,0000	2,1149
1390	99,8722	7,2250	0,0000	2,1141
1395	99,8653	7,3375	0,0000	2,1134
1400	99,8585	7,4500	0,0000	2,1127
1405	99,8516	7,5625	0,0000	2,1119
1410	99,8448	7,6750	0,0000	2,1112
1415	99,8380	7,7875	0,0000	2,1105
1420	99,8312	7,9000	0,0000	2,1097
1425	99,8244	8,0125	0,0000	2,1090
1430	99,8175	8,1250	0,0000	2,1083
1435	99,8108	8,2375	0,0000	2,1076
1440	99,8040	8,3500	0,0000	2,1068
1445	99,7972	8,4625	0,0000	2,1061
1450	99,7904	8,5750	0,0000	2,1054
1455	99,7836	8,6875	0,0000	2,1046
1460	99,7769	8,8000	0,0000	2,1039

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
1465	99,7701	8,9125	0,0000	2,1032
1470	99,7634	9,0250	0,0000	2,1025
1475	99,7566	9,1375	0,0000	2,1017
1480	99,7499	9,2500	0,0000	2,1010
1485	99,7431	9,3625	0,0000	2,1003
1490	99,7364	9,4750	0,0000	2,0996
1495	99,7297	9,5875	0,0000	2,0988
1500	99,7230	9,7000	0,0000	2,0981
1505	99,7163	9,8125	0,0000	2,0974
1510	99,7096	9,9250	0,0000	2,0967
1515	99,7029	10,0375	0,0000	2,0959
1520	99,6962	10,1500	0,0000	2,0952
1525	99,6895	10,2625	0,0000	2,0945
1530	99,6829	10,3750	0,0000	2,0938
1535	99,6762	10,4875	0,0000	2,0930
1540	99,6695	10,6000	0,0000	2,0923
1545	99,6629	10,7125	0,0000	2,0916
1550	99,6563	10,8250	0,0000	2,0909
1555	99,6496	10,9375	0,0000	2,0902
1560	99,6430	11,0500	0,0000	2,0894
1565	99,6364	11,1625	0,0000	2,0887
1570	99,6297	11,2750	0,0000	2,0880
1575	99,6231	11,3875	0,0000	2,0873
1580	99,6165	11,5000	0,0000	2,0866
1585	99,6099	11,6125	0,0000	2,0859
1590	99,6033	11,7250	0,0000	2,0851
1595	99,5967	11,8375	0,0000	2,0844
1600	99,5902	11,9500	0,0000	2,0837
1605	99,5836	12,0625	0,0000	2,0830
1610	99,5770	12,1750	0,0000	2,0823
1615	99,5705	12,2875	0,0000	2,0816
1620	99,5639	12,4000	0,0000	2,0809
1625	99,5574	12,5125	0,0000	2,0801
1630	99,5508	12,6250	0,0000	2,0794
1635	99,5443	12,7375	0,0000	2,0787
1640	99,5378	12,8500	0,0000	2,0780
1645	99,5313	12,9625	0,0000	2,0773
1650	99,5247	13,0750	0,0000	2,0766
1655	99,5182	13,1875	0,0000	2,0759
1660	99,5117	13,3000	0,0000	2,0752
1665	99,5052	13,4125	0,0000	2,0745
1670	99,4988	13,5250	0,0000	2,0737
1675	99,4923	13,6375	0,0000	2,0730
1680	99,4858	13,7500	0,0000	2,0723
1685	99,4793	13,8625	0,0000	2,0716
1690	99,4729	13,9750	0,0000	2,0709
1695	99,4664	14,0875	0,0000	2,0702
1700	99,4600	14,2000	0,0000	2,0695
1705	99,4535	14,3125	0,0000	2,0688
1710	99,4471	14,4250	0,0000	2,0681
1715	99,4407	14,5375	0,0000	2,0674
1720	99,4343	14,6500	0,0000	2,0667
1725	99,4278	14,7625	0,0000	2,0660
1730	99,4214	14,8750	0,0000	2,0653
1735	99,4150	14,9875	0,0000	2,0646
1740	99,4086	15,1000	0,0000	2,0639
1745	99,4022	15,2125	0,0000	2,0632
1750	99,3959	15,3250	0,0000	2,0625
1755	99,3895	15,4375	0,0000	2,0618
1760	99,3831	15,5500	0,0000	2,0611
1765	99,3768	15,6625	0,0000	2,0604
1				

Tablica 1- nastavak 2 Rezultati proračuna za dužinu preljevno praga $B_1 = 2 \text{ m}$

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
1815	99,3135	1,5000	0,0000	2,0534
1820	99,3072	1,5000	0,0000	2,0527
1825	99,3009	1,5000	0,0000	2,0520
1830	99,2947	1,5000	0,0000	2,0513
1835	99,2884	1,5000	0,0000	2,0506
1840	99,2821	1,5000	0,0000	2,0499
1845	99,2759	1,5000	0,0000	2,0493
1850	99,2696	1,5000	0,0000	2,0486
1855	99,2634	1,5000	0,0000	2,0479
1860	99,2571	1,5000	0,0000	2,0472
1865	99,2509	1,5000	0,0000	2,0465
1870	99,2447	1,5000	0,0000	2,0458
1875	99,2385	1,5000	0,0000	2,0451
1880	99,2322	1,5000	0,0000	2,0444
1885	99,2260	1,5000	0,0000	2,0437
1890	99,2198	1,5000	0,0000	2,0431
1895	99,2136	1,5000	0,0000	2,0424
1900	99,2075	1,5000	0,0000	2,0417
1905	99,2013	1,5000	0,0000	2,0410
1910	99,1951	1,5000	0,0000	2,0403
1915	99,1889	1,5000	0,0000	2,0396
1920	99,1828	1,5000	0,0000	2,0389
1925	99,1766	1,5000	0,0000	2,0383
1930	99,1705	1,5000	0,0000	2,0376
1935	99,1643	1,5000	0,0000	2,0369
1940	99,1582	1,5000	0,0000	2,0362
1945	99,1521	1,5000	0,0000	2,0355
1950	99,1460	1,5000	0,0000	2,0348
1955	99,1399	1,5000	0,0000	2,0342
1960	99,1337	1,5000	0,0000	2,0335
1965	99,1276	1,5000	0,0000	2,0328
1970	99,1216	1,5000	0,0000	2,0321
1975	99,1155	1,5000	0,0000	2,0314
1980	99,1094	1,5000	0,0000	2,0308
1985	99,1033	1,5000	0,0000	2,0301
1990	99,0972	1,5000	0,0000	2,0294
1995	99,0912	1,5000	0,0000	2,0287
2000	99,0851	1,5000	0,0000	2,0281
2005	99,0791	1,5000	0,0000	2,0274
2010	99,0730	1,5000	0,0000	2,0267
2015	99,0670	1,5000	0,0000	2,0260
2020	99,0610	1,5000	0,0000	2,0254
2025	99,0549	1,5000	0,0000	2,0247
2030	99,0489	1,5000	0,0000	2,0240
2035	99,0429	1,5000	0,0000	2,0233
2040	99,0369	1,5000	0,0000	2,0227
2045	99,0309	1,5000	0,0000	2,0220
2050	99,0249	1,5000	0,0000	2,0213
2055	99,0189	1,5000	0,0000	2,0207
2060	99,0130	1,5000	0,0000	2,0200
2065	99,0070	1,5000	0,0000	2,0193
2070	99,0010	1,5000	0,0000	2,0186
2075	98,9951	1,5000	0,0000	2,0180
2080	98,9891	1,5000	0,0000	2,0173
2085	98,9832	1,5000	0,0000	2,0166
2090	98,9772	1,5000	0,0000	2,0160
2095	98,9713	1,5000	0,0000	2,0153
2100	98,9654	1,5000	0,0000	2,0146
2105	98,9595	1,5000	0,0000	2,0140
2110	98,9536	1,5000	0,0000	2,0133
2115	98,9476	1,5000	0,0000	2,0126
2120	98,9417	1,5000	0,0000	2,0120
2125	98,9359	1,5000	0,0000	2,0113
2130	98,9300	1,5000	0,0000	2,0107
2135	98,9241	1,5000	0,0000	2,0100
2140	98,9182	1,5000	0,0000	2,0093
2145	98,9123	1,5000	0,0000	2,0087
2150	98,9065	1,5000	0,0000	2,0080
2155	98,9006	1,5000	0,0000	2,0073
2160	98,8948	1,5000	0,0000	2,0067
2165	98,8889	1,5000	0,0000	2,0060
2170	98,8831	1,5000	0,0000	2,0054
2175	98,8773	1,5000	0,0000	2,0047
2180	98,8714	1,5000	0,0000	2,0040
2185	98,8656	1,5000	0,0000	2,0034
2190	98,8598	1,5000	0,0000	2,0027
2195	98,8540	1,5000	0,0000	2,0021
2200	98,8482	1,5000	0,0000	2,0014
2205	98,8424	1,5000	0,0000	2,0008
2210	98,8366	1,5000	0,0000	2,0001
2215	98,8309	1,5000	0,0000	1,9995
2220	98,8251	1,5000	0,0000	1,9988
2225	98,8193	1,5000	0,0000	1,9981
2230	98,8136	1,5000	0,0000	1,9975
2235	98,8078	1,5000	0,0000	1,9968
2240	98,8021	1,5000	0,0000	1,9962
2245	98,7963	1,5000	0,0000	1,9955
2250	98,7906	1,5000	0,0000	1,9949
2255	98,7849	1,5000	0,0000	1,9942
2260	98,7792	1,5000	0,0000	1,9936
2265	98,7734	1,5000	0,0000	1,9929
2270	98,7677	1,5000	0,0000	1,9923
2275	98,7620	1,5000	0,0000	1,9916
2280	98,7563	1,5000	0,0000	1,9910
2285	98,7507	1,5000	0,0000	1,9903
2290	98,7450	1,5000	0,0000	1,9897
2295	98,7393	1,5000	0,0000	1,9891
2300	98,7336	1,5000	0,0000	1,9884
2305	98,7280	1,5000	0,0000	1,9878
2310	98,7223	1,5000	0,0000	1,9871
2315	98,7167	1,5000	0,0000	1,9865
2320	98,7110	1,5000	0,0000	1,9858
2325	98,7054	1,5000	0,0000	1,9852
2330	98,6997	1,5000	0,0000	1,9845
2335	98,6941	1,5000	0,0000	1,9839
2340	98,6885	1,5000	0,0000	1,9833
2345	98,6829	1,5000	0,0000	1,9826
2350	98,6773	1,5000	0,0000	1,9820
2355	98,6717	1,5000	0,0000	1,9813
2360	98,6661	1,5000	0,0000	1,9807
2365	98,6605	1,5000	0,0000	1,9801
2370	98,6549	1,5000	0,0000	1,9794
2375	98,6494	1,5000	0,0000	1,9788
2380	98,6438	1,5000	0,0000	1,9781
2385	98,6382	1,5000	0,0000	1,9775
2390	98,6327	1,5000	0,0000	1,9769
2395	98,6271	1,5000	0,0000	1,9762
2400	98,6216	1,5000	0,0000	1,9756
2405	98,6160	1,5000	0,0000	1,9750
2410	98,6105	1,5000	0,0000	1,9743
2415	98,6050	1,5000	0,0000	1,9737
2420	98,5995	1,5000	0,0000	1,9731
2425	98,5940	1,5000	0,0000	1,9724
2430	98,5885	1,5000	0,0000	1,9718
2435	98,5830	1,5000	0,0000	1,9712
2440	98,5775	1,5000	0,0000	1,9705
2445	98,5720	1,5000	0,0000	1,9699
2450	98,5665	1,5000	0,0000	1,9693
2455	98,5610	1,5000	0,0000	1,9686
2460	98,5556	1,5000	0,0000	1,9680
2465	98,5501	1,5000	0,0000	1,9674
2470	98,5447	1,5000	0,0000	1,9668
2475	98,5392	1,5000	0,0000	1,9661
2480	98,5338	1,5000	0,0000	1,9655
2485	98,5283	1,5000	0,0000	1,9649
2490	98,5229	1,5000	0,0000	1,9643
2495	98,5175	1,5000	0,0000	1,9636
2500	98,5121	1,5000	0,0000	1,9630
2505	98,5067	1,5000	0,0000	1,9624
2510	98,5012	1,5000	0,0000	1,9618
2515	98,4959	1,5000	0,0000	1,9611
2520	98,4905	1,5000	0,0000	1,9605
2525	98,4851	1,5000	0,0000	1,9599
2530	98,4797	1,5000	0,0000	1,9593
2535	98,4743	1,5000	0,0000	1,9586
2540	98,4690	1,5000	0,0000	1,9580
2545	98,4636	1,5000	0,0000	1,9574
2550	98,4582	1,5000	0,0000	1,9568
2555	98,4529	1,5000	0,0000	1,9562
2560	98,4476	1,5000	0,0000	1,9555
2565	98,4422	1,5000	0,0000	1,9549
2570	98,4369	1,5000	0,0000	1,9543
2575	98,4316	1,5000	0,0000	1,9537
2580	98,4263	1,5000	0,0000	1,9531
2585	98,4209	1,5000	0,0000	1,9525
2590	98,4156	1,5000	0,0000	1,9518
2595	98,4103	1,5000	0,0000	1,9512
2600	98,4051	1,5000	0,0000	1,9506
2605	98,3998	1,5000	0,0000	1,9500
2610	98,3945	1,5000	0,0000	1,9494
2615	98,3892	1,5000	0,0000	1,9488
2620	98,3840	1,5000	0,0000	1,9482
2625	98,3787	1,5000	0,0000	1,9476
2630	98,3734	1,5000	0,0000	1,9469
2635	98,3682	1,5000	0,0000	1,9463
2640	98,3629	1,5000	0,0000	1,9457
2645	98,3577	1,5000	0,0000	1,9451
2650	98,3525	1,5000	0,0000	1,9445
2655	98,3473	1,5000	0,0000	1,9439
2660	98,3420	1,5000	0,0000	1,9433
2665	98,3368	1,5000	0,0000	1,9427
2670	98,3316	1,5000	0,0000	1,9421
2675	98,3264	1,5000	0,0000	1,9415
2680	98,3212	1,5000	0,0000	1,9409
2685	98,3161	1,5000	0,0000	1,9403
2690	98,3109	1,5000	0,0000	1,9396
2695	98,3057	1,5000	0,0000	1,9390
2700	98,3005	1,5000	0,0000	1,9384
2705	98,2954	1,5000	0,0000	1,9378
2710	98,2902	1,5000	0,0000	1,9372
2715	98,2851	1,5000	0,0000	1,9366
2720	98,2799	1,5000	0,0000	1,9360
2725	98,2748	1,5000	0,0000	1,9354
2730	98,2697	1,5000	0,0000	1,9348
2735	98,2645	1,5000	0,0000	1,9342
2740	98,2594	1,5000	0,0000	1,9336
2745	98,2543	1,5000	0,0000	1,9330
2750	98,2492	1,5000	0,0000	1,9324
2755	98,2441	1,5000	0,0000	1,9318
2760	98,2390	1,5000	0,0000	1,9312
2765	98,2339	1,5000	0,0000	1,9306
2770	98,2288	1,5000	0,0000	1,9300
2775	98,2238	1,5000	0,0000	1,9294
2780	98,2187	1,5000	0,0000	1,9289
2785	98,2136	1,5000	0,0000	1,9283
2790	98,2086	1,5000	0,0000	1,9277
2795	98,2035	1,5000	0,0000	1,9271
2800	98,1985	1,5000	0,0000	1,9265
2805	98,1934	1,5000	0,0000	1,9259
2810	98,1884	1,5000	0,0000	1,9253
2815	98,1834	1,5000	0,0000	1,9247
2820	98,1784	1,5000	0,0000	1,9241
2825	98,1734	1,5000	0,0000	1,9235
2830	98,1683	1,5000	0,0000	1,9229
2835	98,1633	1,5000	0,0000	1,9223
2840	98,1583	1,5000	0,0000	1,9218
2845	98,1534	1,5		

Tablica 2 Rezultati proračuna za dužinu preljevog praga $B_2 = 3\text{ m}$

t(s)	h(m.n.m.)	Qo(m ³ /s)	Qp(m ³ /s)	Q1(m ³ /s)
0	99,5000	1,5000	0,0000	2,0739
5	99,4936	1,5200	0,0000	2,0732
10	99,4875	1,5400	0,0000	2,0725
15	99,4816	1,5600	0,0000	2,0719
20	99,4759	1,5800	0,0000	2,0713
25	99,4705	1,6000	0,0000	2,0707
30	99,4653	1,6200	0,0000	2,0701
35	99,4603	1,6400	0,0000	2,0695
40	99,4556	1,6600	0,0000	2,0690
45	99,4510	1,6800	0,0000	2,0685
50	99,4468	1,7000	0,0000	2,0681
55	99,4427	1,7200	0,0000	2,0676
60	99,4389	1,7400	0,0000	2,0672
65	99,4353	1,7600	0,0000	2,0668
70	99,4319	1,7800	0,0000	2,0664
75	99,4288	1,8000	0,0000	2,0661
80	99,4259	1,8200	0,0000	2,0658
85	99,4232	1,8400	0,0000	2,0655
90	99,4208	1,8600	0,0000	2,0652
95	99,4186	1,8800	0,0000	2,0650
100	99,4166	1,9000	0,0000	2,0648
105	99,4149	1,9200	0,0000	2,0646
110	99,4133	1,9400	0,0000	2,0644
115	99,4120	1,9600	0,0000	2,0643
120	99,4110	1,9800	0,0000	2,0641
125	99,4101	2,0000	0,0000	2,0640
130	99,4095	2,0200	0,0000	2,0640
135	99,4091	2,0400	0,0000	2,0639
140	99,4090	2,0600	0,0000	2,0639
145	99,4090	2,0800	0,0000	2,0639
150	99,4093	2,1000	0,0000	2,0640
155	99,4099	2,1200	0,0000	2,0640
160	99,4106	2,1400	0,0000	2,0641
165	99,4116	2,1600	0,0000	2,0642
170	99,4128	2,1800	0,0000	2,0643
175	99,4142	2,2000	0,0000	2,0645
180	99,4159	2,2200	0,0000	2,0647
185	99,4177	2,2400	0,0000	2,0649
190	99,4198	2,2600	0,0000	2,0651
195	99,4221	2,2800	0,0000	2,0654
200	99,4247	2,3000	0,0000	2,0656
205	99,4289	2,5850	0,0000	2,0661
210	99,4364	2,8700	0,0000	2,0669
215	99,4471	3,1550	0,0000	2,0681
220	99,4610	3,4400	0,0000	2,0696
225	99,4781	3,7250	0,0000	2,0715
230	99,4984	4,0100	0,0000	2,0737
235	99,5219	4,2950	0,0000	2,0763
240	99,5485	4,5800	0,0000	2,0792
245	99,5783	4,8650	0,0000	2,0824
250	99,6112	5,1500	0,0000	2,0860
255	99,6473	5,4350	0,0000	2,0899
260	99,6864	5,7200	0,0000	2,0942
265	99,7287	6,0050	0,0000	2,0987
270	99,7740	6,2900	0,0000	2,1036
275	99,8224	6,5750	0,0000	2,1088
280	99,8739	6,8600	0,0000	2,1143
285	99,9283	7,1450	0,0000	2,1202
290	99,9858	7,4300	0,0000	2,1263
295	100,0458	7,7150	0,0521	2,1327
300	100,1073	8,0000	0,1868	2,1392
305	100,1683	8,0500	0,3669	2,1456
310	100,2271	8,1000	0,5752	2,1518
315	100,2835	8,1500	0,8024	2,1578
320	100,3375	8,2000	1,0422	2,1634
325	100,3890	8,2500	1,2894	2,1688
330	100,4379	8,3000	1,5404	2,1739
335	100,4844	8,3500	1,7920	2,1788
340	100,5285	8,4000	2,0419	2,1833
345	100,5702	8,4500	2,2884	2,1877

t(s)	h(m.n.m.)	Qo(m ³ /s)	Qp(m ³ /s)	Q1(m ³ /s)
350	100,6096	8,5000	2,5299	2,1917
355	100,6469	8,5500	2,7656	2,1956
360	100,6821	8,6000	2,9945	2,1992
365	100,7154	8,6500	3,2162	2,2027
370	100,7468	8,7000	3,4303	2,2059
375	100,7764	8,7500	3,6365	2,2089
380	100,8044	8,8000	3,8350	2,2118
385	100,8309	8,8500	4,0255	2,2145
390	100,8558	8,9000	4,2084	2,2171
395	100,8794	8,9500	4,3837	2,2195
400	100,9018	9,0000	4,5516	2,2217
405	100,9229	9,0500	4,7124	2,2239
410	100,9429	9,1000	4,8664	2,2259
415	100,9618	9,1500	5,0138	2,2279
420	100,9798	9,2000	5,1550	2,2297
425	100,9969	9,2500	5,2903	2,2314
430	101,0131	9,3000	5,4199	2,2331
435	101,0285	9,3500	5,5442	2,2346
440	101,0432	9,4000	5,6634	2,2361
445	101,0572	9,4500	5,7780	2,2375
450	101,0706	9,5000	5,8880	2,2389
455	101,0834	9,5500	5,9939	2,2402
460	101,0956	9,6000	6,0958	2,2414
465	101,1074	9,6500	6,1941	2,2426
470	101,1187	9,7000	6,2889	2,2437
475	101,1295	9,7500	6,3806	2,2448
480	101,1399	9,8000	6,4692	2,2459
485	101,1500	9,8500	6,5550	2,2469
490	101,1597	9,9000	6,6382	2,2479
495	101,1691	9,9500	6,7190	2,2488
500	101,1782	10,0000	6,7975	2,2498
505	101,1864	9,9125	6,8685	2,2506
510	101,1931	9,8250	6,9272	2,2513
515	101,1985	9,7375	6,9745	2,2518
520	101,2028	9,6500	7,0112	2,2522
525	101,2058	9,5625	7,0382	2,2525
530	101,2079	9,4750	7,0561	2,2527
535	101,2090	9,3875	7,0658	2,2529
540	101,2092	9,3000	7,0677	2,2529
545	101,2086	9,2125	7,0627	2,2528
550	101,2073	9,1250	7,0511	2,2527
555	101,2053	9,0375	7,0336	2,2525
560	101,2027	8,9500	7,0106	2,2522
565	101,1995	8,8625	6,9826	2,2519
570	101,1957	8,7750	6,9500	2,2515
575	101,1915	8,6875	6,9131	2,2511
580	101,1868	8,6000	6,8724	2,2506
585	101,1817	8,5125	6,8281	2,2501
590	101,1762	8,4250	6,7805	2,2496
595	101,1704	8,3375	6,7299	2,2490
600	101,1642	8,2500	6,6766	2,2483
605	101,1577	8,1625	6,6208	2,2477
610	101,1509	8,0750	6,5626	2,2470
615	101,1438	7,9875	6,5024	2,2463
620	101,1365	7,9000	6,4403	2,2456
625	101,1290	7,8125	6,3764	2,2448
630	101,1213	7,7250	6,3108	2,2440
635	101,1133	7,6375	6,2439	2,2432
640	101,1052	7,5500	6,1755	2,2424
645	101,0969	7,4625	6,1060	2,2415
650	101,0884	7,3750	6,0353	2,2407
655	101,0797	7,2875	5,9636	2,2398
660	101,0710	7,2000	5,8910	2,2389
665	101,0620	7,1125	5,8175	2,2380
670	101,0530	7,0250	5,7432	2,2371
675	101,0438	6,9375	5,6683	2,2362
680	101,0345	6,8500	5,5927	2,2352
685	101,0251	6,7625	5,5165	2,2343
690	101,0155	6,6750	5,4398	2,2333
695	101,0059	6,5875	5,3626	2,2323

t(s)	h(m.n.m.)	Qo(m ³ /s)	Qp(m ³ /s)	Q1(m ³ /s)
700	100,9962	6,5000	5,2850	2,2313
705	100,9864	6,4125	5,2070	2,2304
710	100,9764	6,3250	5,1287	2,2293
715	100,9664	6,2375	5,0500	2,2283
720	100,9563	6,1500	4,9711	2,2273
725	100,9462	6,0625	4,8919	2,2263
730	100,9359	5,9750	4,8125	2,2252
735	100,9255	5,8875	4,7329	2,2242
740	100,9151	5,8000	4,6531	2,2231
745	100,9046	5,7125	4,5732	2,2220
750	100,8940	5,6250	4,4932	2,2210
755	100,8834	5,5375	4,4131	2,2199
760	100,8728	5,4500	4,3328	2,2188
765	100,8618	5,3625	4,2525	2,2177
770	100,8509	5,2750	4,1722	2,2165
775	100,8400	5,1875	4,0918	2,2154
780	100,8289	5,1000	4,0114	2,2143
785	100,8178	5,0125	3,9309	2,2132
790	100,8066	4,9250	3,8505	2,2120
795	100,7953	4,8375	3,7701	2,2109
800	100,7840	4,7500	3,6897	2,2097
805	100,7726	4,6625	3,6094	2,2085
810	100,7611	4,5750	3,5291	2,2073
815	100,7495	4,4875	3,4489	2,2062
820	100,7378	4,4000	3,3687	2,2050
825	100,7261	4,3125	3,2887	2,2038
830	100,7143	4,2250	3,2087	2,2025
835	100,7024	4,1375	3,1288	2,2013
840	100,6904	4,0500	3,0490	2,2001
845	100,6783	3,9625	2,9694	2,1988
850	100,6661	3,8750	2,8899	2,1976
855	100,6539	3,7875	2,8105	2,1963
860	100,6415	3,7000	2,7313	2,1950
865	100,6291	3,6125	2,6523	2,1938
870	100,6166	3,5250	2,5734	2,1925
875	100,6039	3,4375	2,4947	2,1912
880	100,5912	3,3500	2,4163	2,1898
885	100,5784	3,2625	2,3380	2,1885
890	100,5654	3,1750	2,2600	2,1872
895	100,5524	3,0875	2,1822	2,1858
900	100,5392	3,0000	2,1047	2,1845
905	100,5263	2,9750	2,0293	2,1831
910	100,5138	2,9500	1,9576	2,1818
915	100,5018	2,9250	1,8893	2,1806
920	100,4902	2,9000	1,8242	2,1794
925	100,4790	2,8750	1,7620	2,1782
930	100,4681	2,8500	1,7025	2,1771
935	100,4576	2,8250	1,6456	2,1760
940	100,4475	2,8000	1,5909	2,1749
945	100,4376	2,7750	1,5385	2,1739
950	100,4279	2,7500	1,4880	2,1729
955	100,4186	2,7250	1,4394	2,1719
960	100,4094	2,7000	1,3926	2,1710
965	100,4005	2,6750	1,3473	2,1700
970	100,3918	2,6500	1,3036	2,1691
975	100,3833	2,6250	1,2613	2,1682
980	100,3749	2,6000	1,2203	2,1674
985	100,3667	2,5750	1,1805	2,1665
990	100,3587	2,5500	1,1419	2,1657
995	100,3508	2,5250	1,1043	2,1648
1000	100,3430	2,5000	1,0678	2,1640
1005	100,3353	2,4750	1,0322	2,1632
1010	100,3278	2,4500	0,9975	2,1624
1015	100,3203	2,		

Tablica 2 – nastavak 1 - Rezultati proračuna za dužinu preljevnog praga $B_2 = 3 \text{ m}$

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
1050	100,2702	2,2500	0,7466	2,1564
1055	100,2633	2,2250	0,7180	2,1557
1060	100,2564	2,2000	0,6899	2,1549
1065	100,2495	2,1750	0,6624	2,1542
1070	100,2426	2,1500	0,6353	2,1535
1075	100,2358	2,1250	0,6086	2,1528
1080	100,2290	2,1000	0,5824	2,1520
1085	100,2222	2,0750	0,5567	2,1513
1090	100,2154	2,0500	0,5313	2,1506
1095	100,2086	2,0250	0,5064	2,1499
1100	100,2018	2,0000	0,4819	2,1492
1105	100,1950	1,9750	0,4577	2,1485
1110	100,1882	1,9500	0,4339	2,1477
1115	100,1814	1,9250	0,4105	2,1470
1120	100,1745	1,9000	0,3875	2,1463
1125	100,1676	1,8750	0,3648	2,1456
1130	100,1607	1,8500	0,3426	2,1448
1135	100,1538	1,8250	0,3207	2,1441
1140	100,1469	1,8000	0,2992	2,1434
1145	100,1399	1,7750	0,2780	2,1426
1150	100,1328	1,7500	0,2573	2,1419
1155	100,1257	1,7250	0,2370	2,1411
1160	100,1186	1,7000	0,2170	2,1404
1165	100,1114	1,6750	0,1976	2,1396
1170	100,1041	1,6500	0,1786	2,1389
1175	100,0968	1,6250	0,1600	2,1381
1180	100,0894	1,6000	0,1420	2,1373
1185	100,0819	1,5750	0,1246	2,1365
1190	100,0743	1,5500	0,1077	2,1357
1195	100,0667	1,5250	0,0915	2,1349
1200	100,0589	1,5000	0,0760	2,1341
1205	100,0511	1,5000	0,0615	2,1332
1210	100,0436	1,5000	0,0483	2,1324
1215	100,0361	1,5000	0,0365	2,1316
1220	100,0288	1,5000	0,0260	2,1309
1225	100,0216	1,5000	0,0168	2,1301
1230	100,0145	1,5000	0,0092	2,1293
1235	100,0074	1,5000	0,0034	2,1286
1240	100,0004	1,5000	0,0000	2,1278
1245	99,9934	1,5000	0,0000	2,1271
1250	99,9865	1,5000	0,0000	2,1264
1255	99,9795	1,5000	0,0000	2,1256
1260	99,9726	1,5000	0,0000	2,1249
1265	99,9656	1,5000	0,0000	2,1241
1270	99,9587	1,5000	0,0000	2,1234
1275	99,9517	1,5000	0,0000	2,1227
1280	99,9448	1,5000	0,0000	2,1219
1285	99,9379	1,5000	0,0000	2,1212
1290	99,9310	1,5000	0,0000	2,1204
1295	99,9241	1,5000	0,0000	2,1197
1300	99,9172	1,5000	0,0000	2,1190
1305	99,9103	1,5000	0,0000	2,1182
1310	99,9034	1,5000	0,0000	2,1175
1315	99,8965	1,5000	0,0000	2,1168
1320	99,8896	1,5000	0,0000	2,1160
1325	99,8828	1,5000	0,0000	2,1153
1330	99,8759	1,5000	0,0000	2,1145
1335	99,8691	1,5000	0,0000	2,1138
1340	99,8622	1,5000	0,0000	2,1131
1345	99,8554	1,5000	0,0000	2,1123
1350	99,8485	1,5000	0,0000	2,1116
1355	99,8417	1,5000	0,0000	2,1109
1360	99,8349	1,5000	0,0000	2,1102
1365	99,8281	1,5000	0,0000	2,1094
1370	99,8213	1,5000	0,0000	2,1087
1375	99,8145	1,5000	0,0000	2,1080
1380	99,8077	1,5000	0,0000	2,1072
1385	99,8009	1,5000	0,0000	2,1065
1390	99,7941	1,5000	0,0000	2,1058
1395	99,7873	1,5000	0,0000	2,1050
1400	99,7806	1,5000	0,0000	2,1043
1405	99,7738	1,5000	0,0000	2,1036
1410	99,7671	1,5000	0,0000	2,1029
1415	99,7603	1,5000	0,0000	2,1021
1420	99,7536	1,5000	0,0000	2,1014
1425	99,7468	1,5000	0,0000	2,1007
1430	99,7401	1,5000	0,0000	2,0999
1435	99,7334	1,5000	0,0000	2,0992
1440	99,7267	1,5000	0,0000	2,0985
1445	99,7200	1,5000	0,0000	2,0978
1450	99,7133	1,5000	0,0000	2,0971
1455	99,7066	1,5000	0,0000	2,0963
1460	99,6999	1,5000	0,0000	2,0956
1465	99,6932	1,5000	0,0000	2,0949
1470	99,6865	1,5000	0,0000	2,0942
1475	99,6799	1,5000	0,0000	2,0934
1480	99,6732	1,5000	0,0000	2,0927
1485	99,6665	1,5000	0,0000	2,0920
1490	99,6599	1,5000	0,0000	2,0913
1495	99,6533	1,5000	0,0000	2,0906
1500	99,6466	1,5000	0,0000	2,0898
1505	99,6400	1,5000	0,0000	2,0891
1510	99,6334	1,5000	0,0000	2,0884
1515	99,6267	1,5000	0,0000	2,0877
1520	99,6201	1,5000	0,0000	2,0870
1525	99,6135	1,5000	0,0000	2,0863
1530	99,6069	1,5000	0,0000	2,0855
1535	99,6004	1,5000	0,0000	2,0848
1540	99,5938	1,5000	0,0000	2,0841
1545	99,5872	1,5000	0,0000	2,0834
1550	99,5806	1,5000	0,0000	2,0827
1555	99,5741	1,5000	0,0000	2,0820
1560	99,5675	1,5000	0,0000	2,0812
1565	99,5610	1,5000	0,0000	2,0805
1570	99,5544	1,5000	0,0000	2,0798
1575	99,5479	1,5000	0,0000	2,0791
1580	99,5413	1,5000	0,0000	2,0784
1585	99,5348	1,5000	0,0000	2,0777
1590	99,5283	1,5000	0,0000	2,0770
1595	99,5218	1,5000	0,0000	2,0763
1600	99,5153	1,5000	0,0000	2,0756
1605	99,5088	1,5000	0,0000	2,0748
1610	99,5023	1,5000	0,0000	2,0741
1615	99,4958	1,5000	0,0000	2,0734
1620	99,4893	1,5000	0,0000	2,0727
1625	99,4829	1,5000	0,0000	2,0720
1630	99,4764	1,5000	0,0000	2,0713
1635	99,4700	1,5000	0,0000	2,0706
1640	99,4635	1,5000	0,0000	2,0699
1645	99,4571	1,5000	0,0000	2,0692
1650	99,4506	1,5000	0,0000	2,0685
1655	99,4442	1,5000	0,0000	2,0678
1660	99,4378	1,5000	0,0000	2,0671
1665	99,4314	1,5000	0,0000	2,0664
1670	99,4249	1,5000	0,0000	2,0657
1675	99,4185	1,5000	0,0000	2,0650
1680	99,4121	1,5000	0,0000	2,0643
1685	99,4057	1,5000	0,0000	2,0636
1690	99,3994	1,5000	0,0000	2,0629
1695	99,3930	1,5000	0,0000	2,0622
1700	99,3866	1,5000	0,0000	2,0615
1705	99,3802	1,5000	0,0000	2,0608
1710	99,3739	1,5000	0,0000	2,0601
1715	99,3675	1,5000	0,0000	2,0594
1720	99,3612	1,5000	0,0000	2,0587
1725	99,3548	1,5000	0,0000	2,0580
1730	99,3485	1,5000	0,0000	2,0573
1735	99,3422	1,5000	0,0000	2,0566
1740	99,3359	1,5000	0,0000	2,0559
1745	99,3296	1,5000	0,0000	2,0552
1750	99,3233	1,5000	0,0000	2,0545
1755	99,3170	1,5000	0,0000	2,0538
1760	99,3107	1,5000	0,0000	2,0531
1765	99,3044	1,5000	0,0000	2,0524
1770	99,2981	1,5000	0,0000	2,0517
1775	99,2918	1,5000	0,0000	2,0510
1780	99,2855	1,5000	0,0000	2,0503
1785	99,2793	1,5000	0,0000	2,0496
1790	99,2730	1,5000	0,0000	2,0489
1795	99,2668	1,5000	0,0000	2,0483
1800	99,2605	1,5000	0,0000	2,0476
1805	99,2543	1,5000	0,0000	2,0469
1810	99,2481	1,5000	0,0000	2,0462
1815	99,2419	1,5000	0,0000	2,0455
1820	99,2356	1,5000	0,0000	2,0448
1825	99,2294	1,5000	0,0000	2,0441
1830	99,2232	1,5000	0,0000	2,0434
1835	99,2170	1,5000	0,0000	2,0427
1840	99,2109	1,5000	0,0000	2,0421
1845	99,2047	1,5000	0,0000	2,0414
1850	99,1985	1,5000	0,0000	2,0407
1855	99,1923	1,5000	0,0000	2,0400
1860	99,1862	1,5000	0,0000	2,0393
1865	99,1800	1,5000	0,0000	2,0386
1870	99,1739	1,5000	0,0000	2,0379
1875	99,1677	1,5000	0,0000	2,0373
1880	99,1616	1,5000	0,0000	2,0366
1885	99,1554	1,5000	0,0000	2,0359
1890	99,1493	1,5000	0,0000	2,0352
1895	99,1432	1,5000	0,0000	2,0345
1900	99,1371	1,5000	0,0000	2,0339
1905	99,1310	1,5000	0,0000	2,0332
1910	99,1249	1,5000	0,0000	2,0325
1915	99,1188	1,5000	0,0000	2,0318
1920	99,1127	1,5000	0,0000	2,0311
1925	99,1066	1,5000	0,0000	2,0305
1930	99,1006	1,5000	0,0000	2,0298
1935	99,0945	1,5000	0,0000	2,0291
1940	99,0884	1,5000	0,0000	2,0284
1945	99,0824	1,5000	0,0000	2,0278
1950	99,0763	1,5000	0,0000	2,0271
1955	99,0703	1,5000	0,0000	2,0264
1960	99,0643	1,5000	0,0000	2,0257
1965	99,0582	1,5000	0,0000	2,0251
1970	99,0522	1,5000	0,0000	2,0244
1975	99,0462	1,5000	0,0000	2,0237
1980	99,0402	1,5000	0,0000	2,0230
1985	99,0342	1,5000	0,0000	2,0224
1990	99,0282	1,5000	0,0000	2,0217
1995	99,0222	1,5000	0,0000	2,0210
2000	99,0162	1,5000	0,0000	2,0204
2005	99,0103	1,5000	0,0000	2,0197
2010	99,0043	1,5000	0,0000	2,0190
2015	98,9983	1,5000	0,0000	2,0183
2020	98,9924	1,5000	0,0000	2,0177
2025	98,9864	1,5000	0,0000	2,0170
2030	98,9805	1,5000	0,0000	2,0163
2035	98,9746	1,5000	0,0000	2,0157
2040	98,9686	1,5000	0,0000	2,0150
2045	98,9627	1,5000	0,0000	2,0143
2050	98,9568	1,5000	0,0000	2,0137
2055	98,9509	1,5000	0,0000	2,0130
2060	98,9450	1,5000	0,0000	2,0123
2065	98,9391	1,5000	0,0000	2,0117
2070	98,9332	1,5000	0,0000	2,0110
2075	98,9273	1,5000	0,0000	

Tablica 2 – nastavak 2 Rezultati proračuna za dužinu preljevnog praga $B_2 = 3\text{ m}$

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
2100	98,8980	1,5000	0,0000	2,0070
2105	98,8921	1,5000	0,0000	2,0064
2110	98,8863	1,5000	0,0000	2,0057
2115	98,8805	1,5000	0,0000	2,0051
2120	98,8746	1,5000	0,0000	2,0044
2125	98,8688	1,5000	0,0000	2,0038
2130	98,8630	1,5000	0,0000	2,0031
2135	98,8572	1,5000	0,0000	2,0024
2140	98,8514	1,5000	0,0000	2,0018
2145	98,8456	1,5000	0,0000	2,0011
2150	98,8398	1,5000	0,0000	2,0005
2155	98,8340	1,5000	0,0000	1,9998
2160	98,8283	1,5000	0,0000	1,9992
2165	98,8225	1,5000	0,0000	1,9985
2170	98,8167	1,5000	0,0000	1,9979
2175	98,8110	1,5000	0,0000	1,9972
2180	98,8052	1,5000	0,0000	1,9965
2185	98,7995	1,5000	0,0000	1,9959
2190	98,7937	1,5000	0,0000	1,9952
2195	98,7880	1,5000	0,0000	1,9946
2200	98,7823	1,5000	0,0000	1,9939
2205	98,7766	1,5000	0,0000	1,9933
2210	98,7709	1,5000	0,0000	1,9926
2215	98,7652	1,5000	0,0000	1,9920
2220	98,7595	1,5000	0,0000	1,9914
2225	98,7538	1,5000	0,0000	1,9907
2230	98,7481	1,5000	0,0000	1,9901
2235	98,7424	1,5000	0,0000	1,9894
2240	98,7367	1,5000	0,0000	1,9888
2245	98,7311	1,5000	0,0000	1,9881
2250	98,7254	1,5000	0,0000	1,9875
2255	98,7198	1,5000	0,0000	1,9868
2260	98,7141	1,5000	0,0000	1,9862
2265	98,7085	1,5000	0,0000	1,9855
2270	98,7028	1,5000	0,0000	1,9849
2275	98,6972	1,5000	0,0000	1,9843
2280	98,6916	1,5000	0,0000	1,9836
2285	98,6860	1,5000	0,0000	1,9830
2290	98,6804	1,5000	0,0000	1,9823
2295	98,6748	1,5000	0,0000	1,9817
2300	98,6692	1,5000	0,0000	1,9811
2305	98,6636	1,5000	0,0000	1,9804
2310	98,6580	1,5000	0,0000	1,9798
2315	98,6524	1,5000	0,0000	1,9791
2320	98,6468	1,5000	0,0000	1,9785
2325	98,6413	1,5000	0,0000	1,9779
2330	98,6357	1,5000	0,0000	1,9772
2335	98,6302	1,5000	0,0000	1,9766
2340	98,6246	1,5000	0,0000	1,9760
2345	98,6191	1,5000	0,0000	1,9753
2350	98,6135	1,5000	0,0000	1,9747
2355	98,6080	1,5000	0,0000	1,9740
2360	98,6025	1,5000	0,0000	1,9734
2365	98,5970	1,5000	0,0000	1,9728
2370	98,5915	1,5000	0,0000	1,9721
2375	98,5860	1,5000	0,0000	1,9715
2380	98,5805	1,5000	0,0000	1,9709
2385	98,5750	1,5000	0,0000	1,9703
2390	98,5695	1,5000	0,0000	1,9696
2395	98,5640	1,5000	0,0000	1,9690
2400	98,5586	1,5000	0,0000	1,9684
2405	98,5531	1,5000	0,0000	1,9677
2410	98,5476	1,5000	0,0000	1,9671
2415	98,5422	1,5000	0,0000	1,9665
2420	98,5367	1,5000	0,0000	1,9659
2425	98,5313	1,5000	0,0000	1,9652
2430	98,5259	1,5000	0,0000	1,9646
2435	98,5204	1,5000	0,0000	1,9640
2440	98,5150	1,5000	0,0000	1,9633
2445	98,5096	1,5000	0,0000	1,9627

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
2450	98,5042	1,5000	0,0000	1,9621
2455	98,4988	1,5000	0,0000	1,9615
2460	98,4934	1,5000	0,0000	1,9609
2465	98,4880	1,5000	0,0000	1,9602
2470	98,4826	1,5000	0,0000	1,9596
2475	98,4773	1,5000	0,0000	1,9590
2480	98,4719	1,5000	0,0000	1,9584
2485	98,4665	1,5000	0,0000	1,9577
2490	98,4612	1,5000	0,0000	1,9571
2495	98,4558	1,5000	0,0000	1,9565
2500	98,4505	1,5000	0,0000	1,9559
2505	98,4451	1,5000	0,0000	1,9553
2510	98,4398	1,5000	0,0000	1,9546
2515	98,4345	1,5000	0,0000	1,9540
2520	98,4292	1,5000	0,0000	1,9534
2525	98,4239	1,5000	0,0000	1,9528
2530	98,4185	1,5000	0,0000	1,9522
2535	98,4132	1,5000	0,0000	1,9516
2540	98,4080	1,5000	0,0000	1,9510
2545	98,4027	1,5000	0,0000	1,9503
2550	98,3974	1,5000	0,0000	1,9497
2555	98,3921	1,5000	0,0000	1,9491
2560	98,3868	1,5000	0,0000	1,9485
2565	98,3816	1,5000	0,0000	1,9479
2570	98,3763	1,5000	0,0000	1,9473
2575	98,3711	1,5000	0,0000	1,9467
2580	98,3658	1,5000	0,0000	1,9461
2585	98,3606	1,5000	0,0000	1,9454
2590	98,3553	1,5000	0,0000	1,9448
2595	98,3501	1,5000	0,0000	1,9442
2600	98,3449	1,5000	0,0000	1,9436
2605	98,3397	1,5000	0,0000	1,9430
2610	98,3345	1,5000	0,0000	1,9424
2615	98,3293	1,5000	0,0000	1,9418
2620	98,3241	1,5000	0,0000	1,9412
2625	98,3189	1,5000	0,0000	1,9406
2630	98,3137	1,5000	0,0000	1,9400
2635	98,3085	1,5000	0,0000	1,9394
2640	98,3034	1,5000	0,0000	1,9388
2645	98,2982	1,5000	0,0000	1,9382
2650	98,2930	1,5000	0,0000	1,9376
2655	98,2879	1,5000	0,0000	1,9370
2660	98,2827	1,5000	0,0000	1,9364
2665	98,2776	1,5000	0,0000	1,9358
2670	98,2725	1,5000	0,0000	1,9352
2675	98,2673	1,5000	0,0000	1,9346
2680	98,2622	1,5000	0,0000	1,9340
2685	98,2571	1,5000	0,0000	1,9334
2690	98,2520	1,5000	0,0000	1,9328
2695	98,2469	1,5000	0,0000	1,9322
2700	98,2418	1,5000	0,0000	1,9316
2705	98,2367	1,5000	0,0000	1,9310
2710	98,2316	1,5000	0,0000	1,9304
2715	98,2265	1,5000	0,0000	1,9298
2720	98,2215	1,5000	0,0000	1,9292
2725	98,2164	1,5000	0,0000	1,9286
2730	98,2113	1,5000	0,0000	1,9280
2735	98,2063	1,5000	0,0000	1,9274
2740	98,2012	1,5000	0,0000	1,9268
2745	98,1962	1,5000	0,0000	1,9262
2750	98,1912	1,5000	0,0000	1,9256
2755	98,1861	1,5000	0,0000	1,9250
2760	98,1811	1,5000	0,0000	1,9244
2765	98,1761	1,5000	0,0000	1,9238
2770	98,1711	1,5000	0,0000	1,9233
2775	98,1661	1,5000	0,0000	1,9227
2780	98,1611	1,5000	0,0000	1,9221
2785	98,1561	1,5000	0,0000	1,9215
2790	98,1511	1,5000	0,0000	1,9209
2795	98,1461	1,5000	0,0000	1,9203

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
2800	98,1411	1,5000	0,0000	1,9197
2805	98,1362	1,5000	0,0000	1,9191
2810	98,1312	1,5000	0,0000	1,9186
2815	98,1263	1,5000	0,0000	1,9180
2820	98,1213	1,5000	0,0000	1,9174
2825	98,1164	1,5000	0,0000	1,9168
2830	98,1114	1,5000	0,0000	1,9162
2835	98,1065	1,5000	0,0000	1,9156
2840	98,1016	1,5000	0,0000	1,9150
2845	98,0966	1,5000	0,0000	1,9145
2850	98,0917	1,5000	0,0000	1,9139
2855	98,0868	1,5000	0,0000	1,9133
2860	98,0819	1,5000	0,0000	1,9127
2865	98,0770	1,5000	0,0000	1,9121
2870	98,0721	1,5000	0,0000	1,9116
2875	98,0673	1,5000	0,0000	1,9110

Tablica 3 Rezultati proračuna za dužinu preljevog praga $B_3 = 4 \text{ m}$

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
0	99,5000	1,5000	0,0000	2,0739
5	99,4936	1,5200	0,0000	2,0732
10	99,4875	1,5400	0,0000	2,0725
15	99,4816	1,5600	0,0000	2,0719
20	99,4759	1,5800	0,0000	2,0713
25	99,4705	1,6000	0,0000	2,0707
30	99,4653	1,6200	0,0000	2,0701
35	99,4603	1,6400	0,0000	2,0695
40	99,4556	1,6600	0,0000	2,0690
45	99,4510	1,6800	0,0000	2,0685
50	99,4468	1,7000	0,0000	2,0681
55	99,4427	1,7200	0,0000	2,0676
60	99,4389	1,7400	0,0000	2,0672
65	99,4353	1,7600	0,0000	2,0668
70	99,4319	1,7800	0,0000	2,0664
75	99,4288	1,8000	0,0000	2,0661
80	99,4259	1,8200	0,0000	2,0658
85	99,4232	1,8400	0,0000	2,0655
90	99,4208	1,8600	0,0000	2,0652
95	99,4186	1,8800	0,0000	2,0650
100	99,4166	1,9000	0,0000	2,0648
105	99,4149	1,9200	0,0000	2,0646
110	99,4133	1,9400	0,0000	2,0644
115	99,4120	1,9600	0,0000	2,0643
120	99,4110	1,9800	0,0000	2,0641
125	99,4101	2,0000	0,0000	2,0640
130	99,4095	2,0200	0,0000	2,0640
135	99,4091	2,0400	0,0000	2,0639
140	99,4090	2,0600	0,0000	2,0639
145	99,4090	2,0800	0,0000	2,0639
150	99,4093	2,1000	0,0000	2,0640
155	99,4099	2,1200	0,0000	2,0640
160	99,4106	2,1400	0,0000	2,0641
165	99,4116	2,1600	0,0000	2,0642
170	99,4128	2,1800	0,0000	2,0643
175	99,4142	2,2000	0,0000	2,0645
180	99,4159	2,2200	0,0000	2,0647
185	99,4177	2,2400	0,0000	2,0649
190	99,4198	2,2600	0,0000	2,0651
195	99,4221	2,2800	0,0000	2,0654
200	99,4247	2,3000	0,0000	2,0656
205	99,4289	2,5850	0,0000	2,0661
210	99,4364	2,8700	0,0000	2,0669
215	99,4471	3,1550	0,0000	2,0681
220	99,4610	3,4400	0,0000	2,0696
225	99,4781	3,7250	0,0000	2,0715
230	99,4984	4,0100	0,0000	2,0737
235	99,5219	4,2950	0,0000	2,0763
240	99,5485	4,5800	0,0000	2,0792
245	99,5783	4,8650	0,0000	2,0824
250	99,6112	5,1500	0,0000	2,0860
255	99,6473	5,4350	0,0000	2,0899
260	99,6864	5,7200	0,0000	2,0942
265	99,7287	6,0050	0,0000	2,0987
270	99,7740	6,2900	0,0000	2,1036
275	99,8224	6,5750	0,0000	2,1088
280	99,8739	6,8600	0,0000	2,1143
285	99,9283	7,1450	0,0000	2,1202
290	99,9858	7,4300	0,0000	2,1263
295	100,0457	7,7150	0,0692	2,1327
300	100,1068	8,0000	0,2472	2,1391
305	100,1668	8,0500	0,4828	2,1455
310	100,2241	8,1000	0,7517	2,1515
315	100,2783	8,1500	1,0407	2,1572
320	100,3295	8,2000	1,3406	2,1626
325	100,3776	8,2500	1,6446	2,1676
330	100,4227	8,3000	1,9477	2,1723
335	100,4648	8,3500	2,2461	2,1767
340	100,5042	8,4000	2,5370	2,1808
345	100,5408	8,4500	2,8184	2,1846

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
350	100,5749	8,5000	3,0892	2,1882
355	100,6066	8,5500	3,3483	2,1914
360	100,6361	8,6000	3,5954	2,1945
365	100,6635	8,6500	3,8303	2,1973
370	100,6890	8,7000	4,0531	2,1999
375	100,7127	8,7500	4,2640	2,2024
380	100,7347	8,8000	4,4634	2,2046
385	100,7553	8,8500	4,6518	2,2068
390	100,7744	8,9000	4,8296	2,2087
395	100,7922	8,9500	4,9975	2,2105
400	100,8089	9,0000	5,1561	2,2123
405	100,8245	9,0500	5,3058	2,2138
410	100,8391	9,1000	5,4474	2,2153
415	100,8528	9,1500	5,5813	2,2167
420	100,8657	9,2000	5,7081	2,2181
425	100,8778	9,2500	5,8283	2,2193
430	100,8892	9,3000	5,9425	2,2205
435	100,9000	9,3500	6,0511	2,2216
440	100,9102	9,4000	6,1545	2,2226
445	100,9199	9,4500	6,2532	2,2236
450	100,9292	9,5000	6,3476	2,2245
455	100,9380	9,5500	6,4380	2,2254
460	100,9464	9,6000	6,5248	2,2263
465	100,9544	9,6500	6,6082	2,2271
470	100,9622	9,7000	6,6887	2,2279
475	100,9696	9,7500	6,7663	2,2286
480	100,9768	9,8000	6,8414	2,2294
485	100,9837	9,8500	6,9142	2,2301
490	100,9904	9,9000	6,9849	2,2308
495	100,9969	9,9500	7,0537	2,2314
500	101,0032	10,0000	7,1208	2,2321
505	101,0087	9,9125	7,1795	2,2326
510	101,0128	9,8250	7,2241	2,2330
515	101,0158	9,7375	7,2558	2,2333
520	101,0177	9,6500	7,2758	2,2335
525	101,0186	9,5625	7,2852	2,2336
530	101,0186	9,4750	7,2852	2,2336
535	101,0178	9,3875	7,2767	2,2335
540	101,0162	9,3000	7,2604	2,2334
545	101,0141	9,2125	7,2372	2,2332
550	101,0113	9,1250	7,2077	2,2329
555	101,0080	9,0375	7,1727	2,2326
560	101,0043	8,9500	7,1326	2,2322
565	101,0001	8,8625	7,0880	2,2317
570	100,9955	8,7750	7,0393	2,2313
575	100,9906	8,6875	6,9870	2,2308
580	100,9853	8,6000	6,9315	2,2302
585	100,9798	8,5125	6,8730	2,2297
590	100,9739	8,4250	6,8119	2,2291
595	100,9679	8,3375	6,7484	2,2285
600	100,9616	8,2500	6,6828	2,2278
605	100,9551	8,1625	6,6154	2,2272
610	100,9484	8,0750	6,5462	2,2265
615	100,9416	7,9875	6,4756	2,2258
620	100,9346	7,9000	6,4036	2,2251
625	100,9275	7,8125	6,3303	2,2244
630	100,9202	7,7250	6,2560	2,2236
635	100,9128	7,6375	6,1808	2,2229
640	100,9053	7,5500	6,1047	2,2221
645	100,8977	7,4625	6,0278	2,2213
650	100,8900	7,3750	5,9502	2,2205
655	100,8822	7,2875	5,8720	2,2197
660	100,8743	7,2000	5,7933	2,2189
665	100,8663	7,1125	5,7141	2,2181
670	100,8582	7,0250	5,6345	2,2173
675	100,8501	6,9375	5,5545	2,2165
680	100,8418	6,8500	5,4742	2,2156
685	100,8336	6,7625	5,3936	2,2148
690	100,8252	6,6750	5,3127	2,2139
695	100,8168	6,5875	5,2316	2,2131

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
700	100,8083	6,5000	5,1503	2,2122
705	100,7998	6,4125	5,0689	2,2113
710	100,7912	6,3250	4,9873	2,2104
715	100,7825	6,2375	4,9056	2,2095
720	100,7738	6,1500	4,8238	2,2087
725	100,7650	6,0625	4,7419	2,2078
730	100,7562	5,9750	4,6600	2,2068
735	100,7473	5,8875	4,5780	2,2059
740	100,7383	5,8000	4,4960	2,2050
745	100,7293	5,7125	4,4140	2,2041
750	100,7202	5,6250	4,3319	2,2032
755	100,7111	5,5375	4,2499	2,2022
760	100,7019	5,4500	4,1679	2,2013
765	100,6927	5,3625	4,0859	2,2003
770	100,6834	5,2750	4,0039	2,1994
775	100,6741	5,1875	3,9220	2,1984
780	100,6646	5,1000	3,8402	2,1974
785	100,6552	5,0125	3,7584	2,1965
790	100,6456	4,9250	3,6766	2,1955
795	100,6360	4,8375	3,5950	2,1945
800	100,6264	4,7500	3,5134	2,1935
805	100,6167	4,6625	3,4320	2,1925
810	100,6069	4,5750	3,3506	2,1915
815	100,5970	4,4875	3,2693	2,1904
820	100,5871	4,4000	3,1882	2,1894
825	100,5771	4,3125	3,1072	2,1884
830	100,5671	4,2250	3,0263	2,1873
835	100,5569	4,1375	2,9456	2,1863
840	100,5467	4,0500	2,8650	2,1852
845	100,5364	3,9625	2,7846	2,1842
850	100,5261	3,8750	2,7043	2,1831
855	100,5156	3,7875	2,6242	2,1820
860	100,5051	3,7000	2,5443	2,1809
865	100,4945	3,6125	2,4646	2,1798
870	100,4838	3,5250	2,3851	2,1787
875	100,4731	3,4375	2,3059	2,1776
880	100,4622	3,3500	2,2268	2,1765
885	100,4512	3,2625	2,1480	2,1753
890	100,4402	3,1750	2,0695	2,1742
895	100,4290	3,0875	1,9913	2,1730
900	100,4177	3,0000	1,9133	2,1718
905	100,4067	2,9150	1,8379	2,1707
910	100,3961	2,8300	1,7667	2,1696
915	100,3860	2,7450	1,6996	2,1685
920	100,3763	2,6600	1,6360	2,1675
925	100,3670	2,5750	1,5757	2,1665
930	100,3581	2,4900	1,5185	2,1656
935	100,3494	2,4050	1,4639	2,1647
940	100,3411	2,3200	1,4119	2,1638
945	100,3331	2,2350	1,3622	2,1630
950	100,3252	2,1500	1,3146	2,1622
955	100,3177	2,0650	1,2689	2,1614
960	100,3103	2,0000	1,2250	2,1606
965	100,3031	1,9350	1,1828	2,1598
970	100,2961	1,8700	1,1421	2,1591
975	100,2893	1,8050	1,1027	2,1584
980	100,2826	1,7400	1,0647	2,1577
985	100,2760	1,6750	1,0278	2,1570
990	100,2696	1,6100	0,9921	2,1563
995	100,2633	1,5450	0,9573	2,1557
1000	100,2570	1,4800	0,9236	2,1550
1005	100,2509	1,4150	0,8907	2,1543
1010	100,2448	1,3500	0,8586	2,1537
1015	100,23			

Tablica 3 – nastavak 1 Rezultati proračuna za dužinu preljevnog praga $B_3 = 4 \text{ m}$

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
1050	100,1984	2,2500	0,6263	2,1488
1055	100,1927	2,2250	0,5997	2,1482
1060	100,1871	2,2000	0,5736	2,1476
1065	100,1815	2,1750	0,5480	2,1470
1070	100,1759	2,1500	0,5227	2,1464
1075	100,1703	2,1250	0,4979	2,1459
1080	100,1646	2,1000	0,4734	2,1453
1085	100,1590	2,0750	0,4494	2,1447
1090	100,1534	2,0500	0,4257	2,1441
1095	100,1477	2,0250	0,4024	2,1435
1100	100,1421	2,0000	0,3795	2,1429
1105	100,1364	1,9750	0,3569	2,1423
1110	100,1307	1,9500	0,3347	2,1417
1115	100,1249	1,9250	0,3129	2,1411
1120	100,1191	1,9000	0,2914	2,1404
1125	100,1133	1,8750	0,2703	2,1398
1130	100,1074	1,8500	0,2496	2,1392
1135	100,1015	1,8250	0,2293	2,1386
1140	100,0956	1,8000	0,2093	2,1380
1145	100,0895	1,7750	0,1899	2,1373
1150	100,0835	1,7500	0,1709	2,1367
1155	100,0773	1,7250	0,1523	2,1360
1160	100,0711	1,7000	0,1343	2,1354
1165	100,0648	1,6750	0,1168	2,1347
1170	100,0584	1,6500	0,1000	2,1340
1175	100,0519	1,6250	0,0838	2,1333
1180	100,0453	1,6000	0,0684	2,1326
1185	100,0386	1,5750	0,0538	2,1319
1190	100,0318	1,5500	0,0403	2,1312
1195	100,0249	1,5250	0,0278	2,1305
1200	100,0178	1,5000	0,0168	2,1297
1205	100,0107	1,5000	0,0078	2,1289
1210	100,0037	1,5000	0,0016	2,1282
1215	99,9967	1,5000	0,0000	2,1274
1220	99,9897	1,5000	0,0000	2,1267
1225	99,9828	1,5000	0,0000	2,1260
1230	99,9758	1,5000	0,0000	2,1252
1235	99,9688	1,5000	0,0000	2,1245
1240	99,9619	1,5000	0,0000	2,1237
1245	99,9550	1,5000	0,0000	2,1230
1250	99,9480	1,5000	0,0000	2,1223
1255	99,9411	1,5000	0,0000	2,1215
1260	99,9342	1,5000	0,0000	2,1208
1265	99,9273	1,5000	0,0000	2,1200
1270	99,9204	1,5000	0,0000	2,1193
1275	99,9135	1,5000	0,0000	2,1186
1280	99,9066	1,5000	0,0000	2,1178
1285	99,8997	1,5000	0,0000	2,1171
1290	99,8928	1,5000	0,0000	2,1164
1295	99,8860	1,5000	0,0000	2,1156
1300	99,8791	1,5000	0,0000	2,1149
1305	99,8723	1,5000	0,0000	2,1142
1310	99,8654	1,5000	0,0000	2,1134
1315	99,8586	1,5000	0,0000	2,1127
1320	99,8517	1,5000	0,0000	2,1120
1325	99,8449	1,5000	0,0000	2,1112
1330	99,8381	1,5000	0,0000	2,1105
1335	99,8313	1,5000	0,0000	2,1098
1340	99,8244	1,5000	0,0000	2,1090
1345	99,8176	1,5000	0,0000	2,1083
1350	99,8108	1,5000	0,0000	2,1076
1355	99,8041	1,5000	0,0000	2,1068
1360	99,7973	1,5000	0,0000	2,1061
1365	99,7905	1,5000	0,0000	2,1054
1370	99,7837	1,5000	0,0000	2,1046
1375	99,7770	1,5000	0,0000	2,1039
1380	99,7702	1,5000	0,0000	2,1032
1385	99,7635	1,5000	0,0000	2,1025
1390	99,7567	1,5000	0,0000	2,1017
1395	99,7500	1,5000	0,0000	2,1010
1400	99,7432	1,5000	0,0000	2,1003
1405	99,7365	1,5000	0,0000	2,0996
1410	99,7298	1,5000	0,0000	2,0988
1415	99,7231	1,5000	0,0000	2,0981
1420	99,7164	1,5000	0,0000	2,0974
1425	99,7097	1,5000	0,0000	2,0967
1430	99,7030	1,5000	0,0000	2,0959
1435	99,6963	1,5000	0,0000	2,0952
1440	99,6896	1,5000	0,0000	2,0945
1445	99,6830	1,5000	0,0000	2,0938
1450	99,6763	1,5000	0,0000	2,0931
1455	99,6696	1,5000	0,0000	2,0923
1460	99,6630	1,5000	0,0000	2,0916
1465	99,6563	1,5000	0,0000	2,0909
1470	99,6497	1,5000	0,0000	2,0902
1475	99,6431	1,5000	0,0000	2,0895
1480	99,6364	1,5000	0,0000	2,0887
1485	99,6298	1,5000	0,0000	2,0880
1490	99,6232	1,5000	0,0000	2,0873
1495	99,6166	1,5000	0,0000	2,0866
1500	99,6100	1,5000	0,0000	2,0859
1505	99,6034	1,5000	0,0000	2,0852
1510	99,5968	1,5000	0,0000	2,0844
1515	99,5903	1,5000	0,0000	2,0837
1520	99,5837	1,5000	0,0000	2,0830
1525	99,5771	1,5000	0,0000	2,0823
1530	99,5706	1,5000	0,0000	2,0816
1535	99,5640	1,5000	0,0000	2,0809
1540	99,5575	1,5000	0,0000	2,0802
1545	99,5509	1,5000	0,0000	2,0794
1550	99,5444	1,5000	0,0000	2,0787
1555	99,5379	1,5000	0,0000	2,0780
1560	99,5313	1,5000	0,0000	2,0773
1565	99,5248	1,5000	0,0000	2,0766
1570	99,5183	1,5000	0,0000	2,0759
1575	99,5118	1,5000	0,0000	2,0752
1580	99,5053	1,5000	0,0000	2,0745
1585	99,4988	1,5000	0,0000	2,0738
1590	99,4924	1,5000	0,0000	2,0731
1595	99,4859	1,5000	0,0000	2,0723
1600	99,4794	1,5000	0,0000	2,0716
1605	99,4730	1,5000	0,0000	2,0709
1610	99,4665	1,5000	0,0000	2,0702
1615	99,4601	1,5000	0,0000	2,0695
1620	99,4536	1,5000	0,0000	2,0688
1625	99,4472	1,5000	0,0000	2,0681
1630	99,4408	1,5000	0,0000	2,0674
1635	99,4343	1,5000	0,0000	2,0667
1640	99,4279	1,5000	0,0000	2,0660
1645	99,4215	1,5000	0,0000	2,0653
1650	99,4151	1,5000	0,0000	2,0646
1655	99,4087	1,5000	0,0000	2,0639
1660	99,4023	1,5000	0,0000	2,0632
1665	99,3960	1,5000	0,0000	2,0625
1670	99,3896	1,5000	0,0000	2,0618
1675	99,3832	1,5000	0,0000	2,0611
1680	99,3768	1,5000	0,0000	2,0604
1685	99,3705	1,5000	0,0000	2,0597
1690	99,3641	1,5000	0,0000	2,0590
1695	99,3578	1,5000	0,0000	2,0583
1700	99,3515	1,5000	0,0000	2,0576
1705	99,3451	1,5000	0,0000	2,0569
1710	99,3388	1,5000	0,0000	2,0562
1715	99,3325	1,5000	0,0000	2,0555
1720	99,3262	1,5000	0,0000	2,0548
1725	99,3199	1,5000	0,0000	2,0541
1730	99,3136	1,5000	0,0000	2,0534
1735	99,3073	1,5000	0,0000	2,0527
1740	99,3010	1,5000	0,0000	2,0520
1745	99,2947	1,5000	0,0000	2,0513
1750	99,2885	1,5000	0,0000	2,0506
1755	99,2822	1,5000	0,0000	2,0500
1760	99,2759	1,5000	0,0000	2,0493
1765	99,2697	1,5000	0,0000	2,0486
1770	99,2635	1,5000	0,0000	2,0479
1775	99,2572	1,5000	0,0000	2,0472
1780	99,2510	1,5000	0,0000	2,0465
1785	99,2448	1,5000	0,0000	2,0458
1790	99,2385	1,5000	0,0000	2,0451
1795	99,2323	1,5000	0,0000	2,0444
1800	99,2261	1,5000	0,0000	2,0437
1805	99,2199	1,5000	0,0000	2,0431
1810	99,2137	1,5000	0,0000	2,0424
1815	99,2075	1,5000	0,0000	2,0417
1820	99,2014	1,5000	0,0000	2,0410
1825	99,1952	1,5000	0,0000	2,0403
1830	99,1890	1,5000	0,0000	2,0396
1835	99,1829	1,5000	0,0000	2,0389
1840	99,1767	1,5000	0,0000	2,0383
1845	99,1706	1,5000	0,0000	2,0376
1850	99,1644	1,5000	0,0000	2,0369
1855	99,1583	1,5000	0,0000	2,0362
1860	99,1522	1,5000	0,0000	2,0355
1865	99,1461	1,5000	0,0000	2,0349
1870	99,1399	1,5000	0,0000	2,0342
1875	99,1338	1,5000	0,0000	2,0335
1880	99,1277	1,5000	0,0000	2,0328
1885	99,1216	1,5000	0,0000	2,0321
1890	99,1156	1,5000	0,0000	2,0315
1895	99,1095	1,5000	0,0000	2,0308
1900	99,1034	1,5000	0,0000	2,0301
1905	99,0973	1,5000	0,0000	2,0294
1910	99,0913	1,5000	0,0000	2,0287
1915	99,0852	1,5000	0,0000	2,0281
1920	99,0792	1,5000	0,0000	2,0274
1925	99,0731	1,5000	0,0000	2,0267
1930	99,0671	1,5000	0,0000	2,0260
1935	99,0611	1,5000	0,0000	2,0254
1940	99,0550	1,5000	0,0000	2,0247
1945	99,0490	1,5000	0,0000	2,0240
1950	99,0430	1,5000	0,0000	2,0233
1955	99,0370	1,5000	0,0000	2,0227
1960	99,0310	1,5000	0,0000	2,0220
1965	99,0250	1,5000	0,0000	2,0213
1970	99,0190	1,5000	0,0000	2,0207
1975	99,0131	1,5000	0,0000	2,0200
1980	99,0071	1,5000	0,0000	2,0193
1985	99,0011	1,5000	0,0000	2,0187
1990	98,9952	1,5000	0,0000	2,0180
1995	98,9892	1,5000	0,0000	2,0173
2000	98,9833	1,5000	0,0000	2,0166
2005	98,9773	1,5000	0,0000	2,0160
2010	98,9714	1,5000	0,0000	2,0153
2015	98,9655	1,5000	0,0000	2,0146
2020	98,9595	1,5000	0,0000	2,0140
2025	98,9536	1,5000	0,0000	2,0133
2030	98,9477	1,5000	0,0000	2,0127
2035	98,9418	1,5000	0,0000	2,0120
2040	98,9359	1,5000	0,0000	2,0113
2045	98,9300	1,5000	0,0000	2,0107
2050	98,9242	1,5000	0,0000	2,0100
2055	98,9183	1,5000	0,0000	2,0093
2060	98,9124	1,5000	0,0000	2,0087
2065	98,9066	1,5000	0,0000	2,0080
2070	98,9007	1,5000	0,0000	2,0074
2075	98,8949	1,5000	0,0000	2,0067</

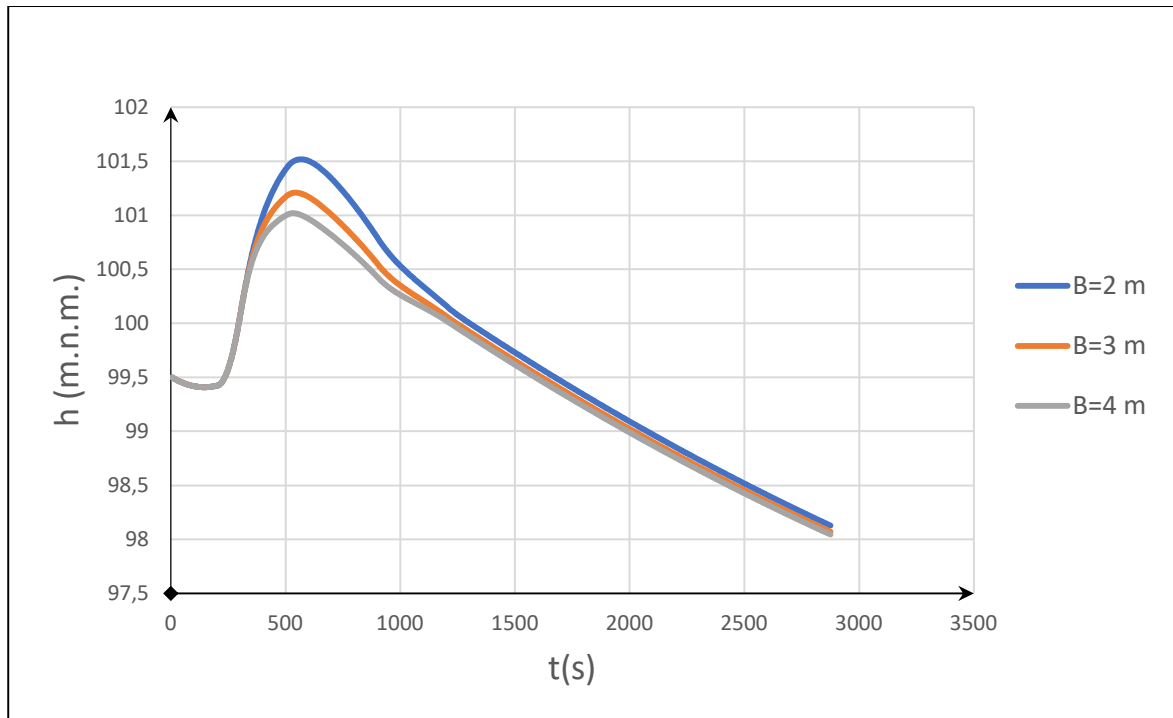
Tablica 3 – nastavak 2 Rezultati proračuna za dužinu preljevnog praga $B_3 = 4 \text{ m}$

t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
2100	98,8657	1,5000	0,0000	2,0034
2105	98,8599	1,5000	0,0000	2,0027
2110	98,8541	1,5000	0,0000	2,0021
2115	98,8483	1,5000	0,0000	2,0014
2120	98,8425	1,5000	0,0000	2,0008
2125	98,8367	1,5000	0,0000	2,0001
2130	98,8309	1,5000	0,0000	1,9995
2135	98,8252	1,5000	0,0000	1,9988
2140	98,8194	1,5000	0,0000	1,9982
2145	98,8137	1,5000	0,0000	1,9975
2150	98,8079	1,5000	0,0000	1,9969
2155	98,8022	1,5000	0,0000	1,9962
2160	98,7964	1,5000	0,0000	1,9955
2165	98,7907	1,5000	0,0000	1,9949
2170	98,7850	1,5000	0,0000	1,9942
2175	98,7792	1,5000	0,0000	1,9936
2180	98,7735	1,5000	0,0000	1,9929
2185	98,7678	1,5000	0,0000	1,9923
2190	98,7621	1,5000	0,0000	1,9917
2195	98,7564	1,5000	0,0000	1,9910
2200	98,7507	1,5000	0,0000	1,9904
2205	98,7450	1,5000	0,0000	1,9897
2210	98,7394	1,5000	0,0000	1,9891
2215	98,7337	1,5000	0,0000	1,9884
2220	98,7280	1,5000	0,0000	1,9878
2225	98,7224	1,5000	0,0000	1,9871
2230	98,7167	1,5000	0,0000	1,9865
2235	98,7111	1,5000	0,0000	1,9858
2240	98,7055	1,5000	0,0000	1,9852
2245	98,6998	1,5000	0,0000	1,9846
2250	98,6942	1,5000	0,0000	1,9839
2255	98,6886	1,5000	0,0000	1,9833
2260	98,6830	1,5000	0,0000	1,9826
2265	98,6774	1,5000	0,0000	1,9820
2270	98,6718	1,5000	0,0000	1,9813
2275	98,6662	1,5000	0,0000	1,9807
2280	98,6606	1,5000	0,0000	1,9801
2285	98,6550	1,5000	0,0000	1,9794
2290	98,6494	1,5000	0,0000	1,9788
2295	98,6439	1,5000	0,0000	1,9782
2300	98,6383	1,5000	0,0000	1,9775
2305	98,6327	1,5000	0,0000	1,9769
2310	98,6272	1,5000	0,0000	1,9762
2315	98,6217	1,5000	0,0000	1,9756
2320	98,6161	1,5000	0,0000	1,9750
2325	98,6106	1,5000	0,0000	1,9743
2330	98,6051	1,5000	0,0000	1,9737
2335	98,5995	1,5000	0,0000	1,9731
2340	98,5940	1,5000	0,0000	1,9724
2345	98,5885	1,5000	0,0000	1,9718
2350	98,5830	1,5000	0,0000	1,9712
2355	98,5775	1,5000	0,0000	1,9705
2360	98,5721	1,5000	0,0000	1,9699
2365	98,5666	1,5000	0,0000	1,9693
2370	98,5611	1,5000	0,0000	1,9687
2375	98,5556	1,5000	0,0000	1,9680
2380	98,5502	1,5000	0,0000	1,9674
2385	98,5447	1,5000	0,0000	1,9668
2390	98,5393	1,5000	0,0000	1,9661
2395	98,5338	1,5000	0,0000	1,9655
2400	98,5284	1,5000	0,0000	1,9649
2405	98,5230	1,5000	0,0000	1,9643
2410	98,5176	1,5000	0,0000	1,9636
2415	98,5121	1,5000	0,0000	1,9630
2420	98,5067	1,5000	0,0000	1,9624
2425	98,5013	1,5000	0,0000	1,9618
2430	98,4959	1,5000	0,0000	1,9611
2435	98,4905	1,5000	0,0000	1,9605
2440	98,4851	1,5000	0,0000	1,9599
2445	98,4798	1,5000	0,0000	1,9593
2450	98,4744	1,5000	0,0000	1,9587
2455	98,4690	1,5000	0,0000	1,9580
2460	98,4637	1,5000	0,0000	1,9574
2465	98,4583	1,5000	0,0000	1,9568
2470	98,4530	1,5000	0,0000	1,9562
2475	98,4476	1,5000	0,0000	1,9556
2480	98,4423	1,5000	0,0000	1,9549
2485	98,4370	1,5000	0,0000	1,9543
2490	98,4316	1,5000	0,0000	1,9537
2495	98,4263	1,5000	0,0000	1,9531
2500	98,4210	1,5000	0,0000	1,9525
2505	98,4157	1,5000	0,0000	1,9519
2510	98,4104	1,5000	0,0000	1,9512
2515	98,4051	1,5000	0,0000	1,9506
2520	98,3998	1,5000	0,0000	1,9500
2525	98,3946	1,5000	0,0000	1,9494
2530	98,3893	1,5000	0,0000	1,9488
2535	98,3840	1,5000	0,0000	1,9482
2540	98,3788	1,5000	0,0000	1,9476
2545	98,3735	1,5000	0,0000	1,9470
2550	98,3683	1,5000	0,0000	1,9463
2555	98,3630	1,5000	0,0000	1,9457
2560	98,3578	1,5000	0,0000	1,9451
2565	98,3526	1,5000	0,0000	1,9445
2570	98,3473	1,5000	0,0000	1,9439
2575	98,3421	1,5000	0,0000	1,9433
2580	98,3369	1,5000	0,0000	1,9427
2585	98,3317	1,5000	0,0000	1,9421
2590	98,3265	1,5000	0,0000	1,9415
2595	98,3213	1,5000	0,0000	1,9409
2600	98,3161	1,5000	0,0000	1,9403
2605	98,3109	1,5000	0,0000	1,9397
2610	98,3058	1,5000	0,0000	1,9391
2615	98,3006	1,5000	0,0000	1,9384
2620	98,2954	1,5000	0,0000	1,9378
2625	98,2903	1,5000	0,0000	1,9372
2630	98,2851	1,5000	0,0000	1,9366
2635	98,2800	1,5000	0,0000	1,9360
2640	98,2749	1,5000	0,0000	1,9354
2645	98,2697	1,5000	0,0000	1,9348
2650	98,2646	1,5000	0,0000	1,9342
2655	98,2595	1,5000	0,0000	1,9336
2660	98,2544	1,5000	0,0000	1,9330
2665	98,2493	1,5000	0,0000	1,9324
2670	98,2442	1,5000	0,0000	1,9318
2675	98,2391	1,5000	0,0000	1,9312
2680	98,2340	1,5000	0,0000	1,9306
2685	98,2289	1,5000	0,0000	1,9301
2690	98,2238	1,5000	0,0000	1,9295
2695	98,2188	1,5000	0,0000	1,9289
2700	98,2137	1,5000	0,0000	1,9283
2705	98,2086	1,5000	0,0000	1,9277
2710	98,2036	1,5000	0,0000	1,9271
2715	98,1986	1,5000	0,0000	1,9265
2720	98,1935	1,5000	0,0000	1,9259
2725	98,1885	1,5000	0,0000	1,9253
2730	98,1835	1,5000	0,0000	1,9247
2735	98,1784	1,5000	0,0000	1,9241
2740	98,1734	1,5000	0,0000	1,9235
2745	98,1684	1,5000	0,0000	1,9229
2750	98,1634	1,5000	0,0000	1,9223
2755	98,1584	1,5000	0,0000	1,9218
2760	98,1534	1,5000	0,0000	1,9212
2765	98,1484	1,5000	0,0000	1,9206
2770	98,1435	1,5000	0,0000	1,9200
2775	98,1385	1,5000	0,0000	1,9194
2780	98,1335	1,5000	0,0000	1,9188
2785	98,1286	1,5000	0,0000	1,9182
2790	98,1236	1,5000	0,0000	1,9177
2795	98,1187	1,5000	0,0000	1,9171

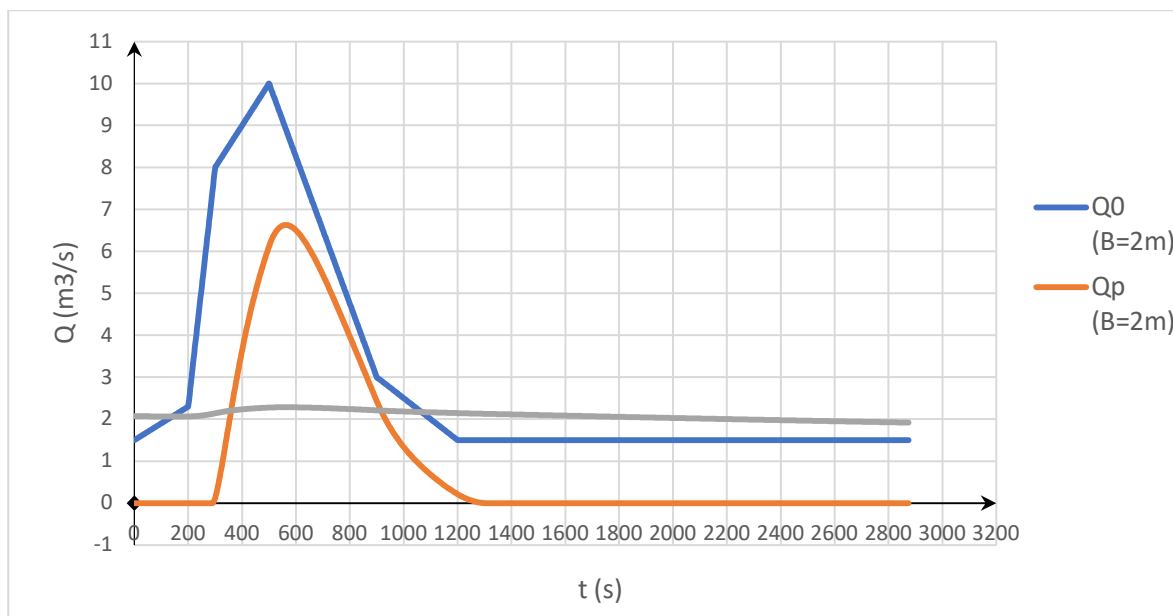
t(s)	h(m.n.m.)	Qo (m ³ /s)	Qp (m ³ /s)	Q1 (m ³ /s)
2800	98,1137	1,5000	0,0000	1,9165
2805	98,1088	1,5000	0,0000	1,9159
2810	98,1039	1,5000	0,0000	1,9153
2815	98,0989	1,5000	0,0000	1,9147
2820	98,0940	1,5000	0,0000	1,9142
2825	98,0891	1,5000	0,0000	1,9136
2830	98,0842	1,5000	0,0000	1,9130
2835	98,0793	1,5000	0,0000	1,9124
2840	98,0744	1,5000	0,0000	1,9118
2845	98,0695	1,5000	0,0000	1,9113
2850	98,0646	1,5000	0,0000	1,9107
2855	98,0598	1,5000	0,0000	1,9101
2860	98,0549	1,5000	0,0000	1,9095
2865	98,0500	1,5000	0,0000	1,9089
2870	98,0452	1,5000	0,0000	1,9084
2875	98,0403	1,5000	0,0000	1,9078

3.3. Grafički prikaz rezultata

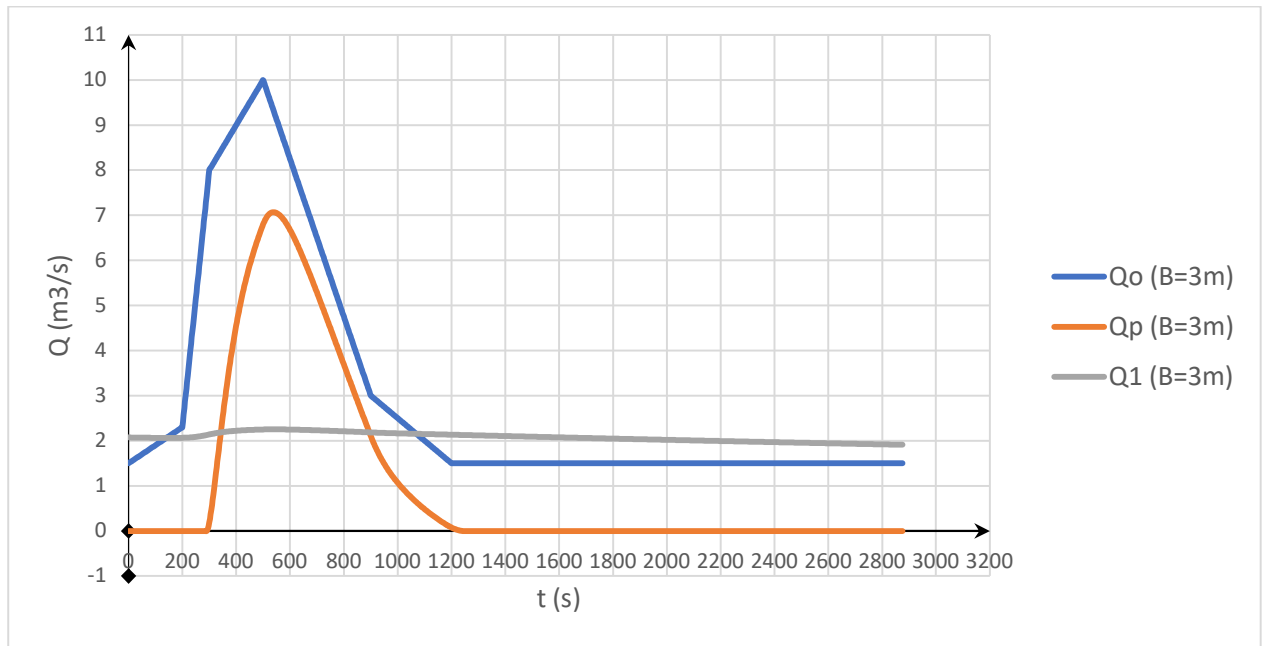
Slika 3 Prikaz vodostaja za B_1, B_2, B_3



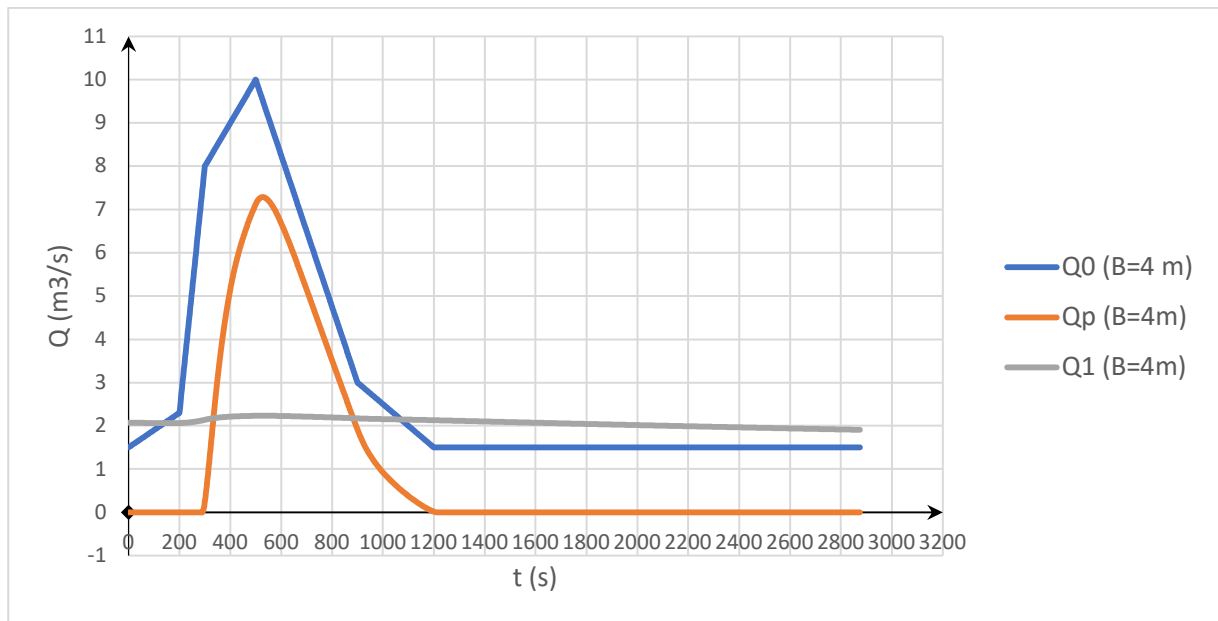
Slika 4 Prikaz dotoka, protoka kroz kratku cijev i preljevnog protoka za širinu preljevnog praga $B=2$ m ovisno o vremenu



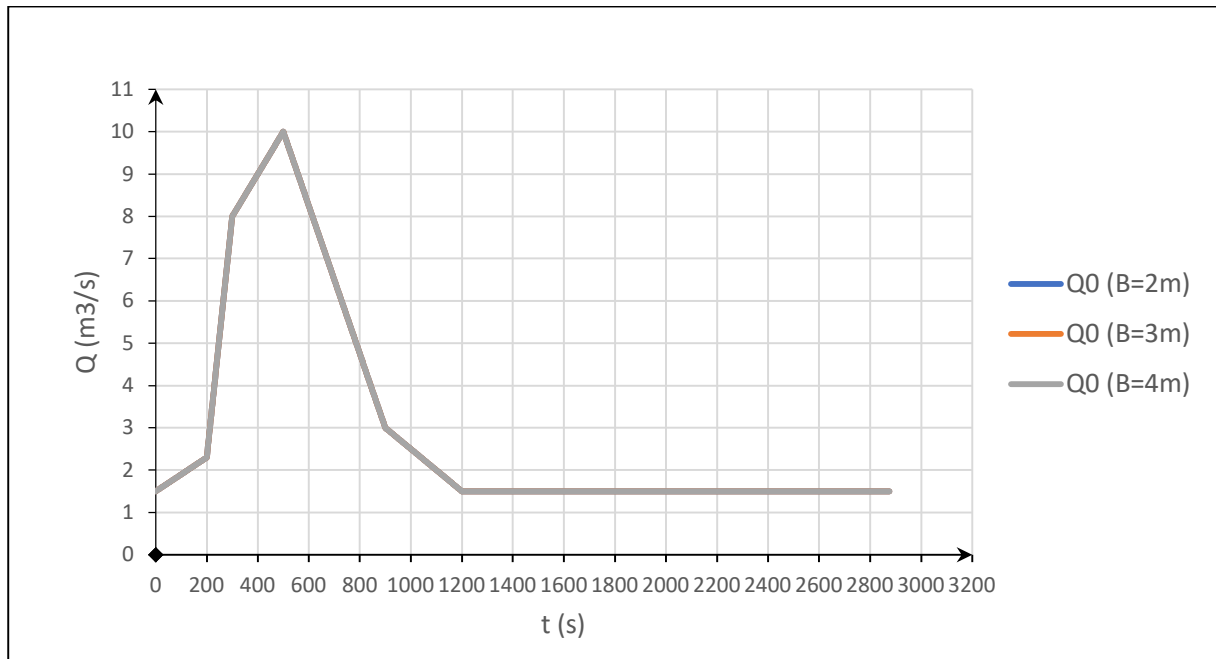
Slika 5 Prikaz dotoka, protoka kroz kratku cijev i preljevnog protoka za širinu preljevnog praga $B=3m$ ovisno o vremenu



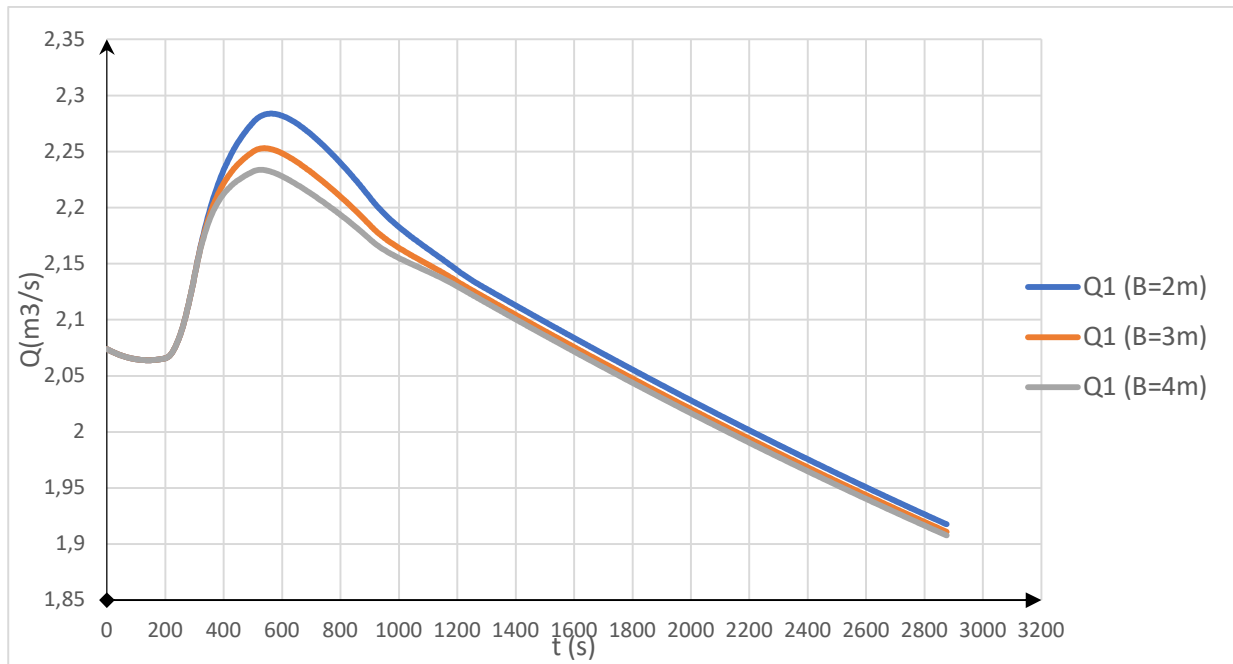
Slika 6 Prikaz dotoka , protoka kroz kratku cijev i preljevnog protoka za širinu preljevnog praga $B=4m$ ovisno o vremenu



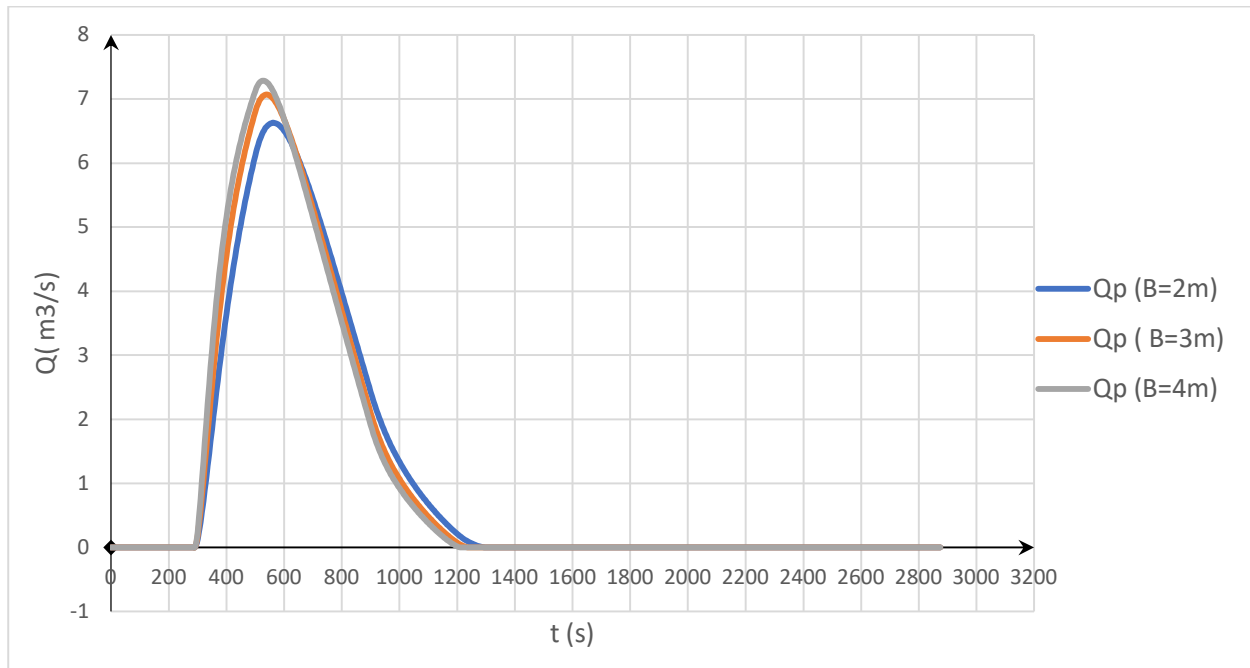
Slika 7 Prikaz dotoka za sve širine preljevnog praga ovisno o vremenu



Slika 8 Prikaz protoka kroz kratku cijev za sve širine preljevnog praga ovisno o vremenu

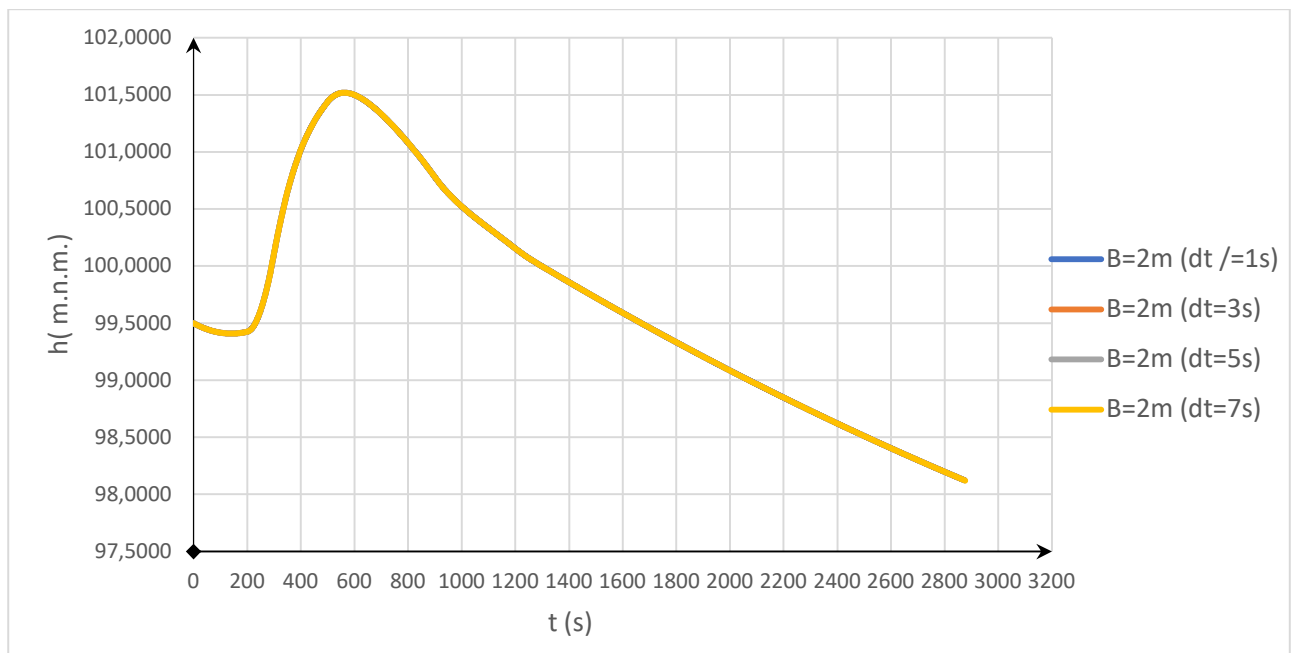


Slika 9 Prikaz preljevnog protoka za sve širine preljevnog praga ovisno o vremenu

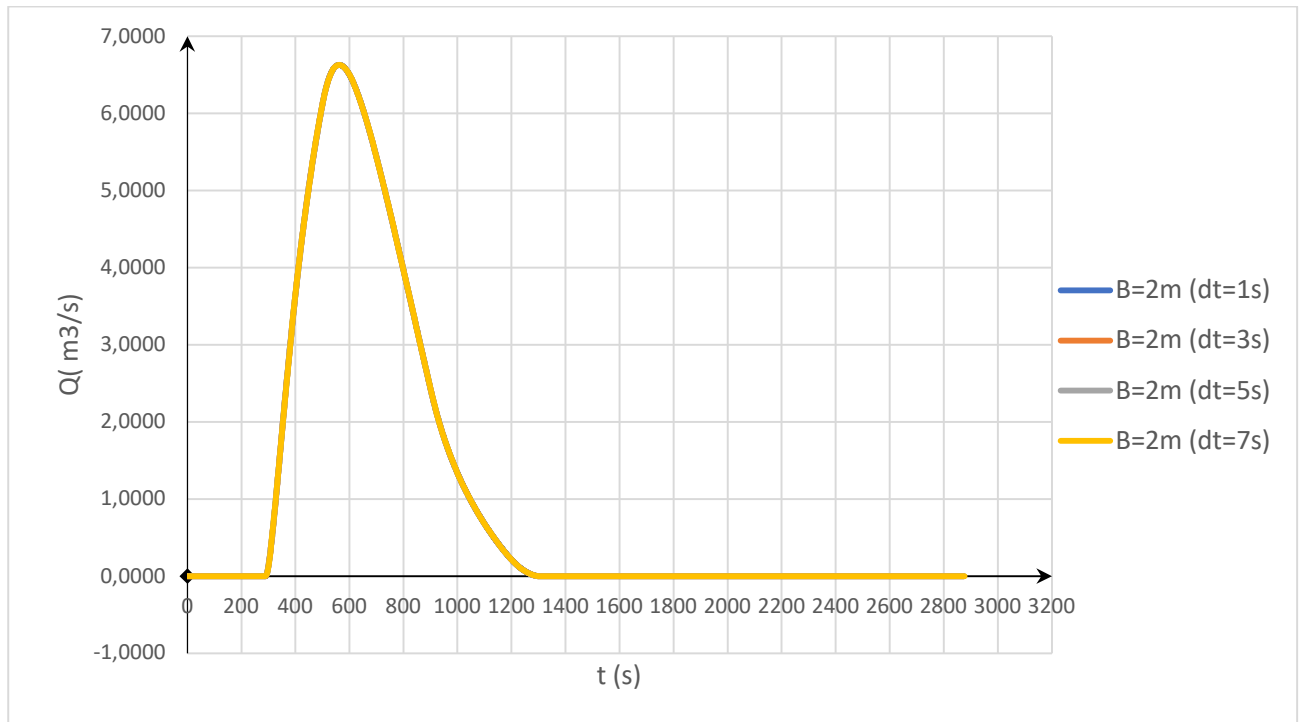


4. Utjecaj vremenskog koraka

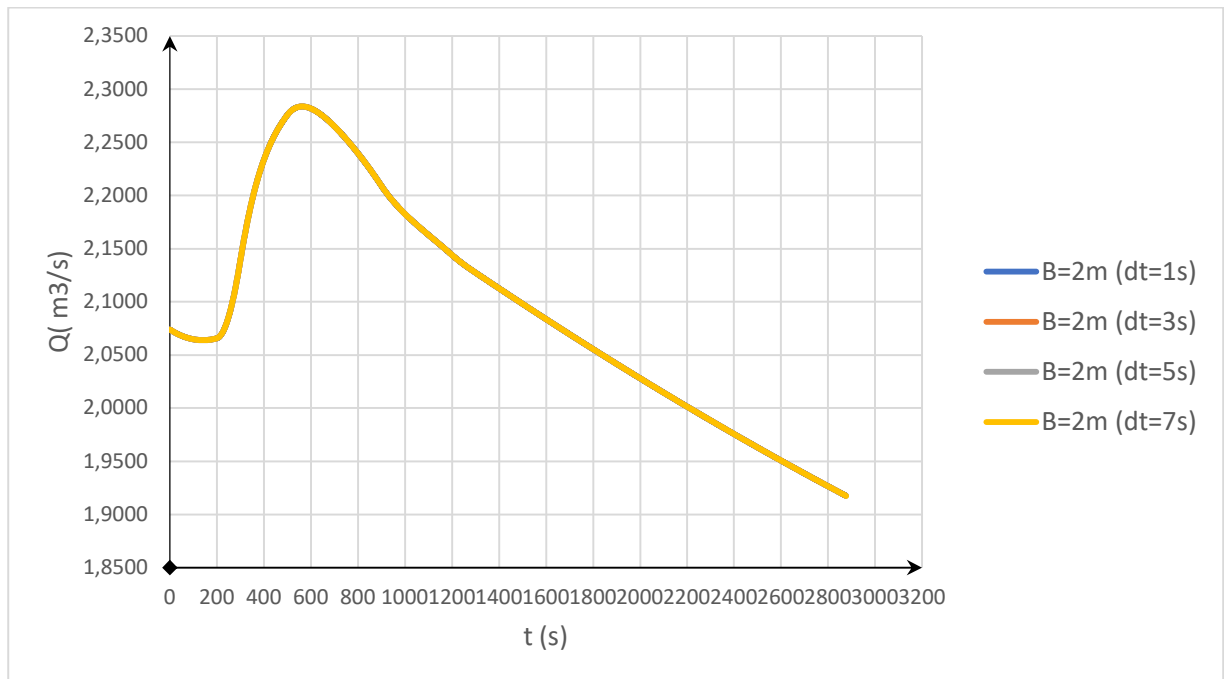
Slika 10 Prikaz vodostaja za $B=2m$ za različite vremenske korake



Slika 11 Prikaz protoka kroz kratku cijev $B=2m$ za različite vremenske korake



Slika 12 Prikaz preljevnog protoka $B=2m$ za različite vremenske korake



Prilikom izrade proračuna za analizu utjecaja vremenskog koraka širine preljevnog praga 2 m u programu Excell bilo je uočljivo da će se dijagrami krivulja u grafičkom dijelu poklopiti, što je i dokazano u priloženim grafovima.

Razlika vodostaja, protoka kroz kratku cijev i preljevnog protoka je minimalna.

5. Zaključak :

Problematika ovog rada odnosila se na otvoreni spremnik s preljevom i ispusnom cijevi površine ovisne o vodostaju. Bilo je potrebno problem riješiti pomoću numeričke integracije mješovitim postupkom koristeći tablični kalkulator Excell. Dobivena su rješenja za 3 varijante dužine preljevnog praga te je istražen utjecaj vremenskog koraka na kvalitetu rješenja.

Na temelju grafičkih prikaza možemo zaključiti sljedeće:

- iz slike 3 vidljivo je da najveće razlike vodostaja za različite širine preljevnog praga nastaju nakon 500-te sekunde te se postupno približavaju jedna drugoj,
- iz slika 4, 5 i 6 na kojima su prikazani rezultati proračuna za sve zadane širine preljevnog praga, uočava se da su razlike u rezultatima očekivane, jer duži preljevni prag omogućava veći preljevni protok, i manje vodostaje u vodospremniku,
- iz slika 10, 11, 12 - također se zaključuje da su razlike minimalne odnosno neprimjetne za različite vremenske korake. To je posljedica primjene mješovitog postupka numeričke integracije koja daje dobre rezultate i kod većih vremenskih intervala.

6. Literatura :

- doc.dr.sc. D. Bojanić, Hidromehanika, Predavanja
- dr.sc. V. Jović, Osnove Hidromehanike, Element, 2006
- dr.sc. S.I. Bradanović, Primjenjena matematika, predavanja